

#### POLITECNICO DI MILANO





#### **Importance Measures**

Masoud Naseri Politecnico di Milano Dipartimento di Energia

masoud.naseri@polimi.it



• **Objective**: Importance Measures (IMs) aim at quantifying the contribution of components or basic events to the measure of system performance of interest

## • Examples:

- **Nuclear**: risk measure (Core Damage Frequency, Large Early Release Frequency)
- Aerospace: unreliability
- **Power generation**: unavailability
- Oil and gas platforms: unavailability
- Why: great practical aid to system designers and managers: trace system bottlenecks and provides guidelines for effective system improvement





## • **How**: *ranking* and *categorization* with respect to:

- risk-significance: if the component failure or unavailability contributes significantly to system risk measure
- safety-significance: if the component plays an important role in the prevention of system undesired states (in system success)

## Hypotheses:

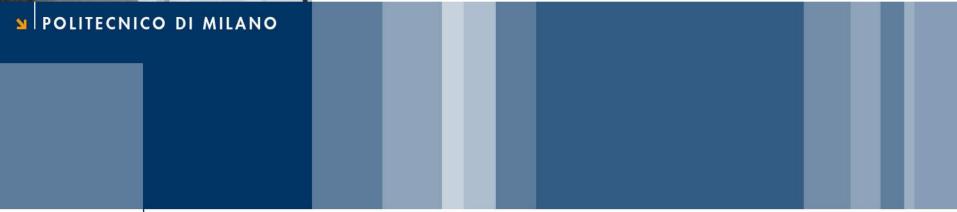
• *n* binary components  $(X_j = 0 \text{ or } 1, j = 1, ..., n)$ 

#### • $X_i = 0$ for component failure

- risk measures adopted: **system reliability** R(t) or failure probability F(t) = 1 R(t)
- $\underline{r}(t) = (r_1(t), r_2(t), ..., r_n(t))$  vector of the reliabilities at time *t* of the individual components
- $R(\underline{r}(t))$  = system reliability









# **Birnbaum's IM**



• Definition

$$I_{j}^{B}(t) = \frac{\partial R(\underline{r}(t))}{\partial r_{j}(t)}$$

- It measures how much a change in the system reliability is due to a change in component j's reliability [differential sensitivity measure]
- Variation of reliability in some components results in the largest variations in system reliability
- Hypotheses:
  - $0 \leq I_j^B(t) \leq 1$
  - All the *n* components must be independent
  - When  $R(\underline{r}(t))$  is a linear function of  $\underline{r}(t)$  and if all components are independent, then  $I_j^B(t)$  does not depend on  $r_j(t)$ , j = 1, 2, ..., n



#### Birnbaum's Importance Measure: Exercise 1

Configuration #	System configuration (system components)	R	$I_1^B$	$I_2^B$	$I_3^B$
Ι	Series (1-2)				
II	Parallel (1-2)				
III	Parallel (1-2-3)				
IV	2-out-of-3 (1-2-3)				



#### Birnbaum's Importance Measure: Exercise 1

Configuration #	System configuration (system components)	R	$I_1^B$	$I_2^B$	$I_3^B$
Ι	Series (1-2)				
Π	Parallel (1-2)				
III	Parallel (1-2-3)				
IV	2-out-of-3 (1-2-3)				

- In a series  $I_i^B(t)$  is larger for less reliable components
- In a **parallel**  $I_j^B(t)$  is larger for **more** reliable components
- In a series  $I_{j}^{B}(t)$  prioritizes components according to *increasing* reliability
- In a **parallel**  $I_j^B(t)$  prioritizes components according to *decreasing* reliability



• Consider various configurations of 3 binary components with  $r_1 = 0.98$ ,  $r_2 = 0.96$ ,  $r_3 = 0.94$ 

Configuration #	System configuration (system components)	R	$I_1^B$	$I_2^B$	$I_3^B$
Ι	Series (1-2)				
II	Parallel (1-2)				
III	Parallel (1-2-3)				
IV	2-out-of-3 (1-2-3)				

Recall:

**Series:** 
$$R(t) = \prod_{i=1}^{N} r_i(t)$$
  
**Parallel:**  $R(t) = 1 - \prod_{i=1}^{N} [1 - r_i(t)]$ 



Series 
$$r_1 - r_2$$
:  $R(t) = \prod_{i=1}^{N} R_i(t) = r_1 r_2$   $I_1^B = \frac{\partial R}{\partial r_1} = r_2$   $I_2^B = \frac{\partial R}{\partial r_2} = r_1$ 

Parallel 
$$r_1 - r_2$$
:  $R(t) = 1 - \prod_{i=1}^{N} [1 - r_i(t)] = r_1 + r_2 - r_1 r_2$ 

$$I_1^B = \frac{\partial R}{\partial r_1} = 1 - r_2$$
  $I_2^B = \frac{\partial R}{\partial r_2} = 1 - r_1$ 



Parallel: 
$$r_1 - r_2 - r_3$$
  $R(t) = 1 - \prod_{i=1}^{N} [1 - r_i(t)] = 1 - (1 - r_1)(1 - r_2)(1 - r_3)$ 

$$R = r_1 + r_2 + r_3 - r_1 r_2 - r_1 r_3 - r_2 r_3 + r_1 r_2 r_3$$

$$I_1^B = \frac{\partial R}{\partial r_1} = 1 - r_2 - r_3 + r_2 r_3$$

$$I_2^B = \frac{\partial R}{\partial r_2} = 1 - r_1 - r_3 + r_1 r_3$$

$$I_{3}^{B} = \frac{\partial R}{\partial r_{3}} = 1 - r_{1} - r_{2} + r_{1}r_{2}$$



2-out-of-3: 
$$r_1 - r_2 - r_3$$
  
 $R = r_1 r_2 + r_1 r_3 + r_2 r_3 - 2r_1 r_2 r_3$ 

$$I_1^B = \frac{\partial R}{\partial r_1} = r_2 + r_3 - 2r_2r_3$$

$$I_2^B = \frac{\partial R}{\partial r_2} = r_1 + r_3 + 2r_1r_3$$

$$I_3^B = \frac{\partial R}{\partial r_3} = r_1 + r_2 + 2r_1r_2$$



Configuration #	System configuration (system components)	R	$I_1^B$	$I_2^B$	$I_3^B$
Ι	Series (1-2)	0.9408	r <sub>2</sub> =0.96	r <sub>1</sub> =0.98	/
II	Parallel (1-2)	0.9992	1- <i>r</i> <sub>2</sub> =0.04	$1 - r_1 = 0.02$	/
III	Parallel (1-2-3)	0.999952	0.0024	0.0012	0.0008
IV	2-out-of-3 (1-2-3)	0.9957	$r_2 + r_3 - 2r_2r_3 = 0.0952$	0.0776	0.0584

- In a series  $I_j^B(t)$  is larger for less reliable components
- In a **parallel**  $I_j^B(t)$  is larger for **more** reliable components
- In a series  $I_j^B(t)$  prioritizes components according to *increasing* reliability
- In a **parallel**  $I_j^B(t)$  prioritizes components according to *decreasing* reliability





$$R_{j}^{+}(t) = R(r_{j} = 1, \underline{r}(t)) = E\left[\Phi\left[\underline{X}(t), X_{j} = 1\right]\right]$$
$$R_{j}^{-}(t) = R(r_{j} = 0, \underline{r}(t)) = E\left[\Phi\left[\underline{X}(t), X_{j} = 0\right]\right]$$



=

## Birnbaum's and Structure Function (2)

$$I_{j}^{B}(t) = \frac{\partial R(\underline{r}(t))}{\partial r_{j}(t)} = R[r_{j} = 1, \underline{r}(t)] - R[r_{j} = 0, \underline{r}(t)] = R_{j}^{+}(t) - R_{j}^{-}(t)$$

 $R_j^+(t) = the increase reliability level with component j perfectly relaible <math>R_j^-(t) = the$  decrease reliability level with component j assumed failed

$$I_{j}^{B}(t) = E\left\{\left[\Phi\left[\underline{X}(t), X_{j}=1\right] - \Phi\left[\underline{X}(t), X_{j}=0\right]\right]\right\}$$
$$= P\left\{\Phi\left[\underline{X}(t), X_{j}=1\right] - \Phi\left[\underline{X}(t), X_{j}=0\right] = 1\right\}$$

$$\Phi\left[\underline{X}(t), X_{j}=1\right] - \Phi\left[\underline{X}(t), X_{j}=0\right] = \{0, 1\}$$

• 
$$I_j^B(t)$$
 is the probability that  $(\underline{X}(t), X_j = 1)$  is a critical path vector, i.e. the other components of the system are in such a state that the system functions if *j* functions and the system is failed if *j* is failed

 $I_j^B(t) = P\{j \text{ is critical}\}$ 



# Birnbaum's Importance Measure: Properties

- $0 \leq I_j^B(t) \leq 1$
- When  $R(\underline{r}(t))$  is a linear function of  $\underline{r}(t)$  and if all components are independent, then  $I_{j}^{B}(t)$  does not depend on  $r_{j}(t)$ , j = 1, 2, ..., n



# Birnbaum's and Structure Function - Example

We know:

$$I_{j}^{B}(t) = E\left\{\left[\Phi\left[\underline{X}(t), X_{j}=1\right] - \Phi\left[\underline{X}(t), X_{j}=0\right]\right]\right\}$$
$$= P\left\{\Phi\left[\underline{X}(t), X_{j}=1\right] - \Phi\left[\underline{X}(t), X_{j}=0\right] = 1\right\}$$

• Consider the series system of components 1 and 2

 $I_1^B = P\{\underline{X} = (1, X_2) \text{ is a critical path vector}\}$ 

It is required that component 2 functions

$$I_1^B = P\{X_2 = 1\} = r_2$$

• Consider the parallel system of component 1 and 2

 $I_1^B = P\{X = (1, X_2) \text{ is a a critical path vector}\}$ 



It is required that component 2 is failed

$$I_1^B = P\{X_2 = 0\} = 1 - r_2$$



• Let us denote the component's unreliability by:

$$q_{j}\left(t\right)=1-r_{j}\left(t\right)$$



$$I_{j}^{B}(t) = \frac{\partial R(\underline{r}(t))}{\partial r_{j}(t)} = R[r_{j} = 1, \underline{r}(t)] - R[r_{j} = 0, \underline{r}(t)] = \frac{\partial F(\underline{q}(t))}{\partial q_{j}(t)} = F[q_{j} = 1, \underline{q}(t)] - F[q_{j} = 0, \underline{q}(t)] = F_{j}^{+}(t) - F_{j}^{-}(t)$$

$$F_{j}^{+}(t) = F\left[q_{j} = 1, \underline{q}(t)\right] = P\left\{\Phi\left[\underline{X}(t), X_{j} = 0\right] = 0\right\}$$
$$F_{j}^{-}(t) = F\left[q_{j} = 0, \underline{q}(t)\right] = P\left\{\Phi\left[\underline{X}(t), X_{j} = 1\right] = 0\right\}$$





• Consider a component *i* characterized by a failure rate  $\lambda_i$ .  $I_i^B(t)$  quantifies how much the system reliability will change by making a small variation of  $\lambda_i$ :

$$\frac{\partial R(r(t))}{\partial \lambda_i} = \frac{\partial R(r(t))}{\partial r_i} \cdot \frac{\partial r_i}{\partial \lambda_i} = I_i^B(t) \frac{\partial r_i(t)}{\partial \lambda_i}$$

- Practical reliability study of a complex system:
  - input parameter estimation (failure rates, repair rates, etc.) = time consuming task



- start with rough estimates
- calculate component Birnbaum's measure of importance

- No extra efforts for finding high-quality data for low importance components
- Improve parameter estimation for high importance components (look for more data,...)





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# **Criticality IM**



• Let  $C[X(t), X_j = 1]$  be the event such that *j* is **critical & works**:

 $P\{C[\underline{X}(t), X_j = 1]\} = I_j^B(t)$ 

• Probability that *j* is **critical** and **failed** at time *t* is:

 $P\{C[\underline{X}(t), X_j = 1] \cap [X_j(t) = 0]\}$ 





• Let  $C[X(t), X_j = 1]$  be the event such that *j* is **critical & works**:

 $P\{C[\underline{X}(t), X_j = 1]\} = I_j^B(t)$ 

• Probability that *j* is **critical** and **failed** at time *t* is:

 $P\{C[\underline{X}(t), X_j = 1] \cap [X_j(t) = 0]\} = I_j^B(t) \cdot (1 - r_j(t))$ 

Component *j* is critical and it fails ≡ Component *j* has caused the system failure





• Let  $C[X(t), X_j = 1]$  be the event such that *j* is **critical & works**:

 $P\{C[\underline{X}(t), X_j = 1]\} = I_j^B(t)$ 

• Probability that *j* is **critical** and **failed** at time *t* is:

$$P\{C[\underline{X}(t), X_j = 1] \cap [X_j(t) = 0]\} = I_j^B(t) \cdot (1 - r_j(t))$$

Component *j* is critical and it fails ≡Component *j* has caused the system failure

• Let us assume that we know that the system is in a failed state at time *t*, we can compute the conditional probability:

$$I_j^{CR}(t) = P\{C[X(t), X_j = 1] \cap [X_j(t) = 0] | \Phi(\underline{X}(t)) = 0\}$$

 $I_j^{CR}(t)$ = Probability that component j has caused the system failure, given that the system is failed at time t





$$I_j^{CR}(t) = P\{C[X(t), X_j = 1] \cap [X_j(t) = 0] | \Phi\left(\underline{X}(t)\right) = 0\}$$
$$= \frac{P\{C[X(t), X_j = 1] \cap [X_j(t) = 0] \cap [\Phi\left(\underline{X}(t)\right) = 0]\}}{P[\Phi\left(\underline{X}(t)\right) = 0]}$$

• 
$$C[\underline{X}(t), X_j = 1] \cap [X_j(t) = 0] \rightarrow$$
 system failure

$$I_{j}^{CR}(t) = \frac{P\{C[X(t), X_{j} = 1] \cap [X_{j}(t) = 0]\}}{1 - R(\underline{r}(t))}$$

•  $P\{C[\underline{X}(t), X_j = 1] \cap [X_j(t) = 0]\} = I_j^B(t) \cdot (1 - r_j(t))$ 

$$I_j^{CR}(t) = \frac{I_j^B(t) \cdot \left(1 - r_j(t)\right)}{1 - R(\underline{r}(t))}$$





 $I_i^{CR}(t) =$ 

Probability that component j has caused the system failure, given that the system is failed at time t

When component *j* is repaired, the system will start functioning again

Probability that if component j is repaired the system will start work, given that the system is failed at time t

•  $I_j^{CR}(t)$  is used to prioritize maintenance actions (e.g. inspections and repairs) in complex systems





Configuration #	System configuration (system components)	$I_1^{cr}$	$I_2^{cr}$	$I_3^{cr}$
I	Series (1-2)			
II	Parallel (1-2)			
Ш	2-out-of-3 (1-2-3)			







Configuration #	System configuration (system components)	$I_1^{cr}$	$I_2^{cr}$	$I_3^{cr}$
Ι	Series (1-2)			
П	Parallel (1-2)			
III	2-out-of-3 (1-2-3)			

- In a series system, the most important component according to *l<sup>cr</sup>* is the least reliable one (=*I<sup>B</sup>*)
- In a simple **parallel**, the criticality of all component is the same (if the system is failed, it will start operates, independently from the component which is repaired)
- In a 2 out of 3 configuration,  $I^{cr}$  increases with decreasing component reliability,  $(\neq I^B)$





- Consider various configurations of 3 binary components with  $r_1 = 0.98$ ,  $r_2 = 0.96$ ,  $r_3 = 0.94$
- Recall the result of the  $I_i^B$  in Exercise 1:

Configuration #	System configuration (system components)	R	$I_1^B$	$I_2^B$	$I_3^B$
Ι	Series (1-2)	0.9408	r <sub>2</sub> =0.96	r <sub>1</sub> =0.98	/
П	Parallel (1-2)	0.9992	1- <i>r</i> <sub>2</sub> =0.04	$1 - r_1 = 0.02$	/
III	Parallel (1-2-3)	0.999952	0.0024	0.0012	0.0008
IV	2-out-of-3 (1-2-3)	0.9957	$r_2 + r_3 - 2r_2r_3 = 0.0952$	0.0776	0.0584

$$Series r_1 - r_2:$$

$$I_1^B(t) \cdot \left(1 - r_j(t)\right)$$

$$I_1^{cr} = \frac{I_1^B(1 - r_1)}{1 - R} = \frac{0.96(1 - 0.98)}{1 - 0.9408} = 0.3243; \quad I_2^{cr} = \frac{I_2^B(1 - r_2)}{1 - R} = \frac{0.98(1 - 0.96)}{1 - 0.9408} = 0.6622$$

Parallel  $r_1 - r_2$ :  $I_1^{cr} = \frac{I_2^B(1 - r_1)}{1 - R} = \frac{0.04(1 - 0.98)}{1 - 0.9992} = 1;$   $I_2^{cr} = \frac{I_2^B(1 - r_2)}{1 - R} = \frac{0.02(1 - 0.96)}{1 - 0.9992} = 1$ 

 $I_j^{CR}$ 

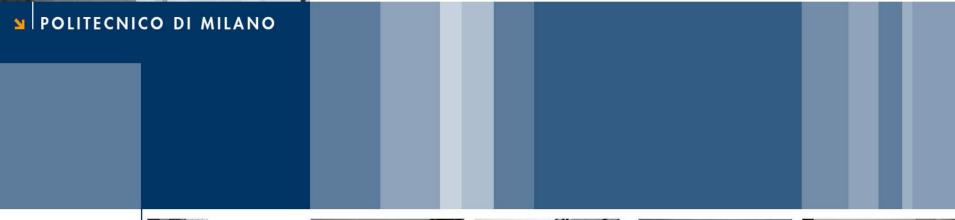
## **Exercise 2: Criticality - Solution**

Configuration #	System configuration (system components)	$I_1^{cr}$	$I_2^{cr}$	$I_3^{cr}$
Ι	Series (1-2)	$\frac{I_1^B(1-r_1)}{1-r_1r_2} = 0.3243$	$\frac{I_2^B \left(1-r_2\right)}{1-r_1 r_2} = 0.662$	/
П	Parallel (1-2)	$\frac{I_1^B (1-r_1)}{1-r_1-r_2+r_1r_2} = 1$	1	/
Π	Parallel (1-2-3)	1	1	1
IV	2-out-of-3 (1-2-3)	0.4428	0.7219	0.8149

- In a series system, the most important component according to *I<sup>cr</sup>* is the least reliable one (=*I<sup>B</sup>*)
- In a simple **parallel**, the criticality of all component is the same (if the system is failed, it will start operates, independently from the component which is repaired)
- In a 2 out of 3 configuration,  $I^{cr}$  increases with decreasing component reliability,  $(\neq I^B)$









# **Fussel-Vesely's IM**



- The component contributes to system failure when a minimal cut set (mcs) containing the component occurs
- >  $I_j^{FV}(t)$  = probability that at least one mcs containing *j* is verified at time *t*, given that the system is failed at *t*

> Let:

- $m_j$  = number of mcs containing component j, j = 1, 2, ..., n
- M<sup>j</sup><sub>h</sub> = {h-th mcs among those containing component j is verified at time t}
- D<sub>j</sub>(t) = event that {at least one mcs that contains component j is verified at time t }:

$$D_j(t) = M_1^j(t) \cup M_2^j(t) \cup \cdots \cup M_{m_j}^j(t)$$



## Fussel-Vesely importance measure (2)

• 
$$I_{j}^{FV}(t) = P\left\{D_{j}(t) \mid \Phi\left[\underline{X}(t)\right] = 0\right\} = \frac{P\left\{D_{j}(t) \cap \Phi\left[\underline{X}(t)\right] = 0\right\}}{P\left\{\Phi\left[\underline{X}(t)\right] = 0\right\}} = \frac{P\left\{D_{j}(t)\right\}}{P\left\{\Phi\left[\underline{X}(t)\right] = 0\right\}}$$

- Hypotheses for a rough approximation:
  - Independent components  $\longrightarrow P(M_h^j(t)) = \prod_{l \in M_h^j} (1 r_l(t))$
  - Independence of cut-sets containing  $j \rightarrow P(D^{j}(t)) \cong 1 \prod_{h=1}^{m_{j}} \left(1 P\left(M_{h}^{j}(t)\right)\right)$

$$I_{j}^{FV}(t) \cong \frac{1 - \prod_{h=1}^{m_{j}} \left(1 - P\left(M_{h}^{j}(t)\right)\right)}{1 - R(\underline{r}(t))}$$

Rare-event approximation

$$I_{j}^{FV}(t) \cong \frac{\sum_{h=1}^{m_{j}} P\left(M_{h}^{j}(t)\right)}{1 - R\left(\underline{r}\left(t\right)\right)} = \frac{F(t) - F_{J}^{-}(t)}{F(t)}$$

F(t) = the present (nominal) failure (Unreliability) level $F_j^-(t) = the decreased failure (Unreliability) level with component j perfectly relaible$ 



Configuration #	System configuration (system components)	$I_1^{FV}$	$I_2^{FV}$	$I_3^{FV}$
Ι	Series (1-2)			
II	Parallel (1-2)			
III	Parallel (1-2-3)			
IV	2-out-of-3 (1-2-3)			







Configuration #	System configuration (system components)	$I_1^{FV}$	$I_2^{FV}$	$I_3^{FV}$
Ι	Series (1-2)			
II	Parallel (1-2)			
III	Parallel (1-2-3)			
IV	2-out-of-3 (1-2-3)			

- Value similar to *I<sup>cr</sup>*: both aim at quantifying the contribution of the failure of component *j* to the system failure probability
- In the **parallel** system configuration, the system itself constitutes a minimal cut set  $\rightarrow I_1^{FV} = I_2^{FV} = 1$ .



### **Exercise 3:** Fussel-Vesely – Solution

- Consider various configurations of 3 binary components with  $r_1 = 0.98$ ,  $r_2 = 0.96$ ,  $r_3 = 0.94$
- Recall:

Series 
$$r_1 - r_2$$
:  $R(t) = r_1 r_2$   
 $F(t) = 1 - r_1 r_2$   $r_2 = r_1 r_2 = r_1 r_2$ 

Parallel 
$$r_1 - r_2$$
:  $R(t) = r_1 + r_2 - r_1 r_2$ 

$$F(t) = 1 - (r_1 + r_2 - r_1 r_2)$$
   
  $F(t) = q_1 q_2$ 

Parallel  $r_1 - r_2 - r_3$ :  $R(t) = r_1 + r_2 + r_3 - r_1r_2 - r_1r_3 - r_2r_3 + r_1r_2r_3$  $F(t) = 1 - (r_1 + r_2 + r_3 - r_1r_2 - r_1r_3 - r_2r_3 + r_1r_2r_3)$   $F(t) = q_1q_2q_3$ 



## **Exercise 3:** Fussel-Vesely – Solution

Series 
$$r_1 - r_2$$
:  $F(t) = q_1 + q_2 - q_1 q_2$   $F_1^-(t) = q_2$   $F_2^-(t) = q_1$ 

$$I_1^{FV}(t) = \frac{F(t) - F_1^-(t)}{F(t)} = \frac{q_1 + q_2 - q_1 q_2 - q_2}{F(t)} = \frac{q_1 - q_1 q_2}{F(t)} \approx \frac{q_1}{1 - R(t)} = \frac{1 - r_1}{1 - r_1 r_2} = 0.3378$$

$$I_2^{FV}(t) = \frac{F(t) - F_2^{-}(t)}{F(t)} = \frac{q_1 + q_2 - q_1 q_2 - q_1}{F(t)} = \frac{q_2 - q_1 q_2}{F(t)} \approx \frac{q_2}{1 - R(t)} = \frac{1 - r_2}{1 - r_1 r_2} = 0.6757$$

Parallel 
$$r_1 - r_2$$
:  $F(t) = q_1 q_2$   $F_1^-(t) = 0$   $F_2^-(t) = 0$ 

$$I_1^{FV}(t) = \frac{F(t) - F_1^{-}(t)}{F(t)} = \frac{q_1 q_2 - 0}{F(t)} = \frac{q_1 q_2}{F(t)} = \frac{q_1 q_2}{q_1 q_2} = 1$$





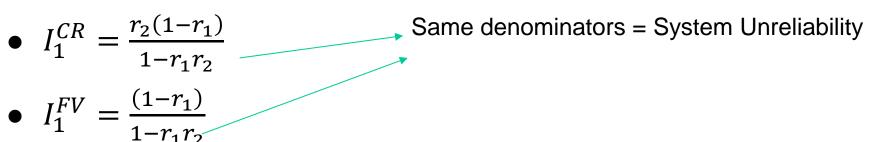
Configuration #	System configuration (system components)	$I_1^{FV}$	$I_2^{FV}$	$I_3^{FV}$
Ι	Series (1-2)	$\frac{1-r_1}{1-r_1r_2} = 0.3378$	$\frac{1-r_2}{1-r_1r_2} = 0.6757$	/
П	Parallel (1-2)	1	1	/
Ш	Parallel (1-2-3)	1	1	1
III	2-out-of-3 (1-2-3)	0.4651	0.7442	0.8372

- Value similar to *I<sup>cr</sup>*: both aim at quantifying the contribution of the failure of component *j* to the system failure probability
- In the **parallel** system configuration, the system itself constitutes a minimal cut set  $\rightarrow I_1^{FV} = I_2^{FV} = 1$ .





• Consider the difference between  $I_1^{CR}$  and  $I_1^{FV}$  for the series:



**Different Numerators!** 

- FV: component 1 contributes to the system failure when it fails (its single component cut set is verified), independently from the state of component 2
- CR: component 1 contributes to the risk only when it is component 1 that causes the system failure, i.e. it is failed but component 2 is working

FV Importance measure takes into account that a component may contribute to the system risk measure without being critical





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# Risk Achievement Worth (RAW) IM & Risk Reduction Worth (RRW) IM



- Problem: which is the worth of a component in achieving the present risk?
- Method: remove the component and then determine how much the risk is increased
- Definition:

$$RAW_{j}(t) = \frac{F\left[q_{j}=1,\underline{q}(t)\right]}{F(t)} = \frac{F_{j}^{+}(t)}{F(t)}$$

F(t) = the present (nominal) failure (Unreliability) level $F_j^+(t) = the increased failure (Unreliability) level with component j always failed$ 

Ratio of the risk when component *j* is considered **always failed** in (0,t)  $(q_j = 1, X_j = 0)$  and the current value of risk

- The RAW is also known by the term **risk increase factor**.
- It highlights the importance of maintaining the current level of reliability of component j
- It is used for maintenance and surveillance decisions.
- Appropriate for **temporary** changes, may be misleading for **permanent** changes (often not complete unavailability).





1

- Problem: which is the worth of a component in reducing the present risk?
- Method: "optimize" the component and then determine how much the risk is decreased
- Definition:

$$RRW_{j}(t) = \frac{F(t)}{F\left[q_{j}(t) = 0, \underline{q}(t)\right]} = \frac{F(t)}{F_{j}^{-}(t)}$$

 $F_j^-(t) = the \ decreased failure \ (Unreliability) level \ with \ component \ j \ perfectly \ relaible$ 

Ratio of the current value of risk and the risk when component j is always available in (0,t)  $(q_j = 0, X_j = 1)$ 

- The RRW is known also by the term **risk decrease factor**.
- It measures the potential of component *j* in reducing the risk
- Useful for identifying or optimizing improvements towards risk reduction (e.g. useful in plant upgrading programs and backfitting activities)





• Consider various configurations of 3 binary components with  $r_1 = 0.98$ ,  $r_2 = 0.96$ ,  $r_3 = 0.94$ 

Configuration #	System configuration (system components)	RAW <sub>1</sub>	RAW <sub>2</sub>	RAW <sub>3</sub>
Ι	Series (1-2)			
II	Parallel (1-2)			
III	2-out-of-3 (1-2-3)			

Configuration #	System configuration (system components)	RRW <sub>1</sub>	RRW <sub>2</sub>	RRW <sub>3</sub>
Ι	Series (1-2)			
II	Parallel (1-2)			
III	2-out-of-3 (1-2-3)			



• Consider various configurations of 3 binary components with  $r_1 = 0.98$ ,  $r_2 = 0.96$ ,  $r_3 = 0.94$ 

#### • Recall:

Series  $r_1 - r_2$ :  $F(t) = q_1 + q_2 - q_1 q_2$ 

Parallel  $r_1 - r_2$ :  $F(t) = q_1 q_2$ 

**Parallel**  $r_1 - r_2 - r_3$ :  $F(t) = q_1 q_2 q_3$ 

$$RAW_j(t) = \frac{F_j^+(t)}{F(t)} \qquad \qquad RRW_j(t) = \frac{F(t)}{F_j^-(t)}$$



Consider various configurations of 3 binary components with r<sub>1</sub> = 0.98, r<sub>2</sub> = 0.96, r<sub>3</sub> = 0.94
FOR:

Series 
$$r_1 - r_2$$
:  $F(t) = q_1 + q_2 - q_1 q_2$   
 $F_1^+(t) = 1 + q_2 - 1, q_2 = 1$   $F_1^-(t) = q_2$   
 $F_2^+(t) = q_1 + 1 - q_1, 1 = 1$   $F_2^-(t) = q_1$   
 $RAW_1(t) = \frac{F_1^+(t)}{F(t)} = \frac{1}{q_1 + q_2 - q_1 q_2} = \frac{1}{(1 - 0.98) + (1 - 0.96) - (1 - 0.98)(1 - 0.96)} = 16.89$ 

$$RAW_2(t) = \frac{F_2^+(t)}{F(t)} = \frac{1}{q_1 + q_2 - q_1q_2} = 16.89$$

$$RRW_{1}(t) = \frac{F(t)}{F_{1}^{-}(t)} = \frac{q_{1} + q_{2} - q_{1}q_{2}}{q_{2}} = 1.48 \qquad RRW_{2}(t) = \frac{F(t)}{F_{2}^{-}(t)} = \frac{q_{1} + q_{2} - q_{1}q_{2}}{q_{1}} = 2.96$$

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Consider various configurations of 3 binary components with r<sub>1</sub> = 0.98, r<sub>2</sub> = 0.96, r<sub>3</sub> = 0.94
FOR:

Parallel 
$$r_1 - r_2$$
:  $F(t) = q_1 q_2$   
 $F_1^+(t) = 1, q_2 = q_2$   $F_1^-(t) = 0$   
 $F_2^+(t) = q_1, 1 = q_1$   $F_2^-(t) = 0$   
 $RAW_1(t) = \frac{F_1^+(t)}{F(t)} = \frac{q_2}{q_1 q_2} = \frac{1}{q_1} = \frac{1}{(1 - 0.98)} = 50$   
 $RAW_2(t) = \frac{F_2^+(t)}{F(t)} = \frac{q_1}{q_1 q_2} = \frac{1}{q_2} = \frac{1}{(1 - 0.96)} = 25$   
 $RRW_1(t) = \frac{F(t)}{F(t)} = \frac{q_1 q_2}{q_1 q_2} = \infty$   $RRW_2(t) = \frac{F(t)}{F(t)} = \frac{q_1 q_2}{q_1 q_2} = \infty$ 

$$RRW_{1}(t) = \frac{F(t)}{F_{1}^{-}(t)} = \frac{q_{1}q_{2}}{0} = \infty \qquad RRW_{2}(t) = \frac{F(t)}{F_{2}^{-}(t)} = \frac{q_{1}q_{2}}{0} =$$



• Consider various configurations of 3 binary components with  $r_1 = 0.98$ ,  $r_2 = 0.96$ ,  $r_3 = 0.94$ 

Configuration #	System configuration (system components)	RAW <sub>1</sub>	RAW <sub>2</sub>	RAW <sub>3</sub>	
Ι	Series (1-2)	$\frac{1}{q_1 + q_2 - q_1 q_2} = 16.89$	$\frac{1}{q_1 + q_2 - q_1 q_2} = 16.89$	/	
Π	Parallel (1-2)	$\frac{q_2}{q_1 q_2} = \frac{1}{q_1} = 50$	$\frac{1}{q_2} = 25$	/	largest if the most reliable component is taken out of service
III	2-out-of-3 (1-2-3)	22.67	18.31	13.75	
Configuration #	System configuration (system components)	RRW <sub>1</sub>	RRW <sub>2</sub>	RRW <sub>3</sub>	
Ι	Series (1-2)	$\frac{q_1 + q_2 - q_1 q_2}{q_2} = 1.48$	$\frac{q_1 + q_2 - q_1 q_2}{q_1} = 2.96$	/	Largest for the components which contribute most to the system failure, i.e, the least reliable
Π	Parallel (1-2)	$\frac{q_1q_2}{0} = \infty$	$\frac{q_1q_2}{0} = \infty$	/	
III	2-out-of-3 (1-2-3)	1.79	3.58	5.38	

- In a **series**, components have the same RAW and are ranked by RRW in increasing order of failure probability
- In a **parallel**, components have the same RRW and are ranked by RAW in decreasing order of failure probability
- In a **parallel** the achievement in risk (RAW) is highest if the most reliable component is **taken out of service**
- In a series the reduction in risk (RRW) achievable by improving the component to perfection is highest for the components which contribute most to the system failure, i.e, the least reliable





Which IMs are more appropriate to rank or categorize components by risk-significance or by safety-significance?

• Let us write the risk metric *F*:  $F(t) = q_j(t) \cdot \left(F_j^+(t) - F_j^-(t)\right) + F_j^-(t) \quad \text{pivotal decomposition}$ 

$$F = \alpha_j \cdot q_j + \beta_j$$

•  $q_j$  = unavailability of j

 $\alpha_j = F_j^+ - F_j^-$  coefficient of  $q_j$  in the risk equation  $\beta_j = F_j^-$  collection of all the other terms of *F* with  $q_j = 0$ 





Fussel-Vesely

$$I_j^{FV} \approx \frac{F - F_j^-}{F} = \frac{\alpha_j q_j + \beta_j - \beta_j}{\alpha_j q_j + \beta_j} = \frac{\alpha_j q_j}{\alpha_j q_j + \beta_j}$$

► High risk installation (very redundant) → failure of a single component is typically not critical →  $\alpha_j q_j \ll \beta_j$ 

$$I_j^{FV} \approx \frac{\alpha_j}{\beta_j} q_j$$

- proportional to the unreliability of component j
- It represents the contribution of component j to risk

How much the component failure/unavailability is contributing to the systerm risk?



# Fussel-Vesely = risk significance IM

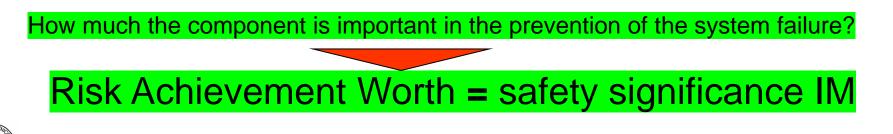




**Risk Achievement Worth:** 

$$RAW_j = \frac{F_j^+}{F} = \frac{\alpha_j + \beta_j}{\alpha_j q_j + \beta_j}$$

- ► High risk installation (very redundant) → failure of a single component is typically not critical → α<sub>j</sub>q<sub>j</sub> ≪ β<sub>j</sub>  $RAW_j \approx \frac{\alpha_j}{\beta_i} + 1$
- >  $RAW_j$  is independent on  $q_j$  → degree of defence against failure provided by the rest of the installation
- A large *RAW<sub>j</sub>* means component *j* is highly safety-significant since the risk increase due to the unavailability of the component is high *→* prevention!





- Birnbaum → appropriate for establishing test and maintenance programs (jointly to RAW to assess the impact in terms of loss of safety of taking the component out of service)
- Fussel-Vesely and Birnbaum → appropriate for the system design phase:
  - *I<sup>FV</sup>* is used for selecting the components candidate for improvement because most contributing to the risk
  - *I<sup>B</sup>* allows identifying for which components the improvements are more effective
- Criticality → appropriate for identifying components most probably causing system failure (help set up a repair priority checklist)





- 1. IMs deal with changes in risk only **at the extremes (0,1)** of the defined ranges of probability
- 2. IMs rank only individual components or basic events, whereas they are not directly applicable to combinations or groups (e.g. change in technical specifications or component's failures made up of more basic events)
- 3. IMs have been mainly applied to systems made up of binary components (i.e. functioning or faulty)
- 4. IMs have been mainly applied to systems made up of binary components (i.e. functioning or faulty)

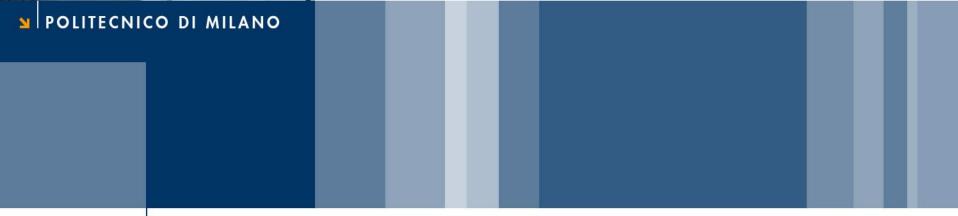
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#### **Generalized Importance Measure**









# **Generalized Importance Measure**



Consider the following relative change in risk due to a change in the probability of the basic failure event *j* from the value q<sub>j</sub> to the value q<sup>n</sup><sub>j</sub>

Pivotal Decomposition:

$$F(t) = F_{j}^{-}(t) + q_{j}(t) \cdot (F_{j}^{+}(t) - F_{j}^{-}(t))$$

$$F_{j}^{n}(t) = F_{j}^{-}(t) + q_{j}^{n}(t) \cdot (F_{j}^{+}(t) - F_{j}^{-}(t)) \cdot \frac{\Delta F_{j}}{F} = \frac{F_{j}^{n} - F}{F} = \frac{(F_{j}^{+}(t) - F_{j}^{-}(t)) \cdot (q_{j}^{n} - q_{j})}{F}$$

$$I_{j}^{G}(q_{j}^{n}) = \frac{F_{j}^{n}}{F} = \{F[q_{j} = 1, \underline{q}(t)] - F[q_{j} = 0, \underline{q}(t)]\} \left(\frac{q_{j}^{n} - q_{j}}{F}\right) + 1$$

$$Risk Impact Curve$$

$$I_{j}^{G}(q_{j}^{n}) = \frac{F_{j}^{n}}{F} = I_{j}^{cr}\left(\frac{q_{j}^{n}}{q_{j}}\right) + \frac{1}{RRW_{j}}$$



- No simple relation between the importance measures of single components and a group  $\rightarrow$  **no general approach!**
- Let us consider the indicator variable T of the top event of a given fault tree can be written as:

 $T = AB(C_1 + C_3) + DE(C_2 + C_4) + F(C_1 + C_3)(C_2 + C_4) + GH$ 

 $(C_k, k = 1, ..., 4 \text{ are different failure modes of component C or different components in the }$ same group)  $C_{1} = 1$ 

 $RAW(C_1) = \frac{F_j^+}{F} = \frac{AB(1+C_3) + DE(C_2+C_4) + F(1+C_3)(C_2+C_4) + GH}{AB(C_1+C_3) + DE(C_2+C_4) + F(C_1+C_3)(C_2+C_4) + GH}$ 

- Substitute  $C_i = 1$ ? **NO**: a value of 2 appears in structure function
- Adding RAWs for basic events? **NO**
- Substitute  $C_i = C$  and Boolean reduction and C = 1? **YES**

$$T = ABC + DEC + FC + GH$$
  

$$RAW(C) = \frac{AB + DE + F + GH}{AB(C_1 + C_3) + DE(C_2 + C_4) + F(C_1 + C_3)(C_2 + C_4) + GH}$$



• Birnbaum:

$$I_{j}^{B} = F\left[q_{j} = 1, \underline{q}(t)\right] - F\left[q_{j} = 0, \underline{q}(t)\right]$$

• Substitute  $C_i = 1$  with **no** Boolean reduction?

$$I_C^B = 2AB + 2DE + 4F$$

• Substitute  $C_i = C$  and Boolean reduction and C = 1?

$$I_C^B = AB + DE + F$$

- Both are unappropriate!
- Fussel-Vesely:

$$I_{C}^{FV}(C) = \frac{AB(C_{1}+C_{3}) + DE(C_{2}+C_{4}) + F(C_{1}+C_{3})(C_{2}+C_{4})}{AB(C_{1}+C_{3}) + DE(C_{2}+C_{4}) + F(C_{1}+C_{3})(C_{2}+C_{4}) + GH}$$

- Any cutset with a contribution from any  $C_k$  of the group is included!
- Already appropriate measure of group importance!
- No additivity ((i.e., not equal to the summation of all individual measures  $I_{C_k}$ )





#### • Differential Importance measure (DIM) :

- Sensitivity measure that ranks the parameters of the risk model according to the fraction of the total change in the risk that is due to a small change in the parameters' values, taken one at a time
- Additivity!

 $F = F(p_1, p_2, ..., p_{Np})$  $dF = \frac{\partial F}{\partial p_1} \cdot dp_1 + \frac{\partial F}{\partial p_2} \cdot dp_2 + ... + \frac{\partial F}{\partial p_{N_p}} \cdot dp_{N_p}$  $\underbrace{\frac{\partial F}{\partial p_i} \cdot dp_i}_{\text{DIM}} \left(p_i\right) = \frac{dF_{p_i}}{dF} = \frac{\frac{\partial F}{\partial p_1} \cdot dp_1 + \frac{\partial F}{\partial p_2} \cdot dp_2 + ... + \frac{\partial F}{\partial p_{N_p}} \cdot dp_{N_p}}{\frac{\partial F}{\partial p_1} \cdot dp_1 + \frac{\partial F}{\partial p_2} \cdot dp_2 + ... + \frac{\partial F}{\partial p_{N_p}} \cdot dp_{N_p}}$ 





• *F* and *F<sub>j</sub>*- are to be considered as random variables characterized by given probability distributions



• IMs is a random variable for which specific statistics can be calculated!







• Extensions to multi-state systems!



