### **Monte Carlo Simulation**

\*\*\*\*\*\*\*\*\*\*

POLITECNICO

1863

\*\*\*\*\*\*\*\*\*\*\*\*

\*\*\*\*\*\*

31.03.2025 | Luca Pinciroli



\*\*\*\*\*\*\*\*\*\*

11111

-1111

DI MILANO



\*\*\*\*\*

### CONTENTS

Sampling

Evaluation of definite integrals

Simulation of system transport

Simulation for reliability/availability analysis

### CONTENTS

### Sampling

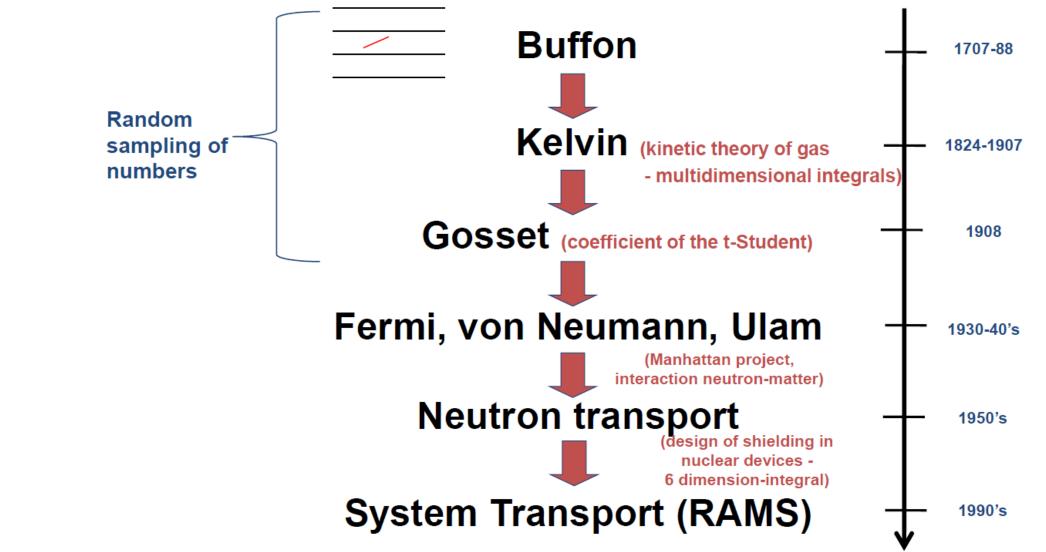
Evaluation of definite integrals

Simulation of system transport

Simulation for reliability/availability analysis



### The history of Monte Carlo simulation



POLITECNICO

ได้วัดเ

#### **Buffon's needle**

Buffon considered a set of parallel straight lines a distance D apart onto a plane and computed the probability P that a needle of length L < D randomly positioned on the plane would intersect one of these lines.

$$P = P\{Y \le Lsin\theta\}$$

$$P = P\{Y \le Lsin\theta\} = \int_{0}^{Lsin\theta} f_{Y}(y) dy = \int_{0}^{Lsin\theta} \frac{1}{D} dy = \frac{Lsin\theta}{D}$$
For a random value of  $\theta \rightarrow joint pdf$  of  $(y, \theta)$ :
$$P = \int_{\theta=0}^{\pi} \int_{y=0}^{Lsin\theta} f_{Y,\theta}(y, \theta) dy d\theta = \int_{\theta=0}^{\pi} \frac{1}{D} d\theta \int_{y=0}^{Lsin\theta} \frac{1}{D} dy = \int_{\theta=0}^{\pi} \frac{Lsin\theta}{\pi D} d\theta = \frac{2L}{\pi D}$$

D

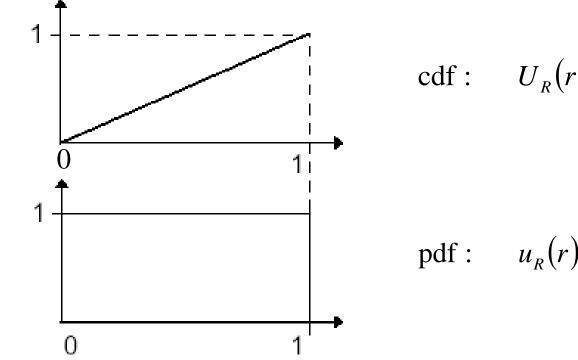
0

1

lasar

POLITECNICO

### Sampling (pseudo) Random Numbers Uniform Distribution



df: 
$$U_R(r) = P\{R \le r\} = r$$

odf: 
$$u_R(r) = \frac{dU_R(r)}{dr} = 1$$



### The Random Number Book (1955)

#### 1 million random numbers

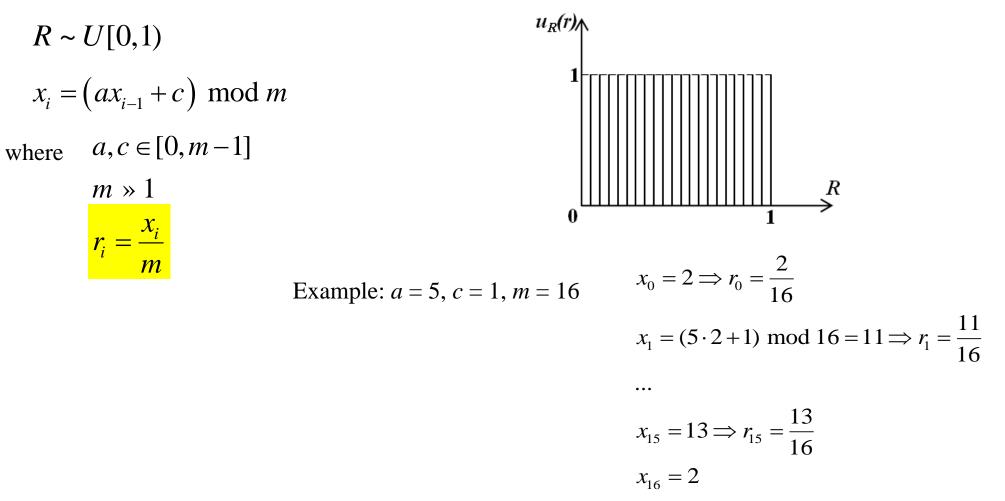
45963	78134	63873
58303	90708	20025
23851	27965	62394
62570	64775	78428
26440	20422	05720
47174	76866	14330
34378	08730	56522
22466	81978	57323
66207	11698	99314
80827	53867	37797
27601	62686	44711
87442	50033	14021
54043	46176	42391
32792	87989	72248
28220	12444	71840
	58303 23851 62570 26440 47174 34378 22466 66207 80827 27601 87442 54043 32792	58303       90708         23851       27965         62570       64775         26440       20422         47174       76866         34378       08730         22466       81978         66207       11698         80827       53867         27601       62686         87442       50033         54043       46176         32792       87989



7

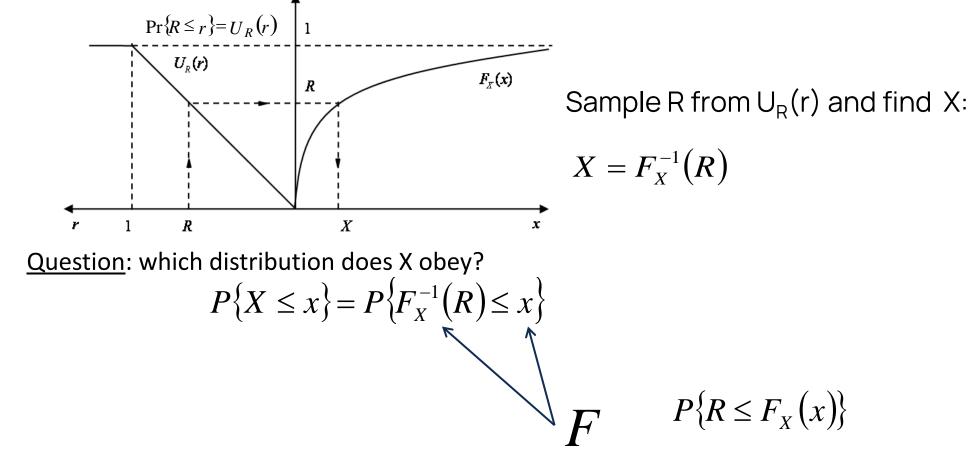
Luca Pinciroli, Department of Energy

### Sampling (pseudo) Random Numbers from Uniform Distribution: Linear Congruential Generator (LCG)





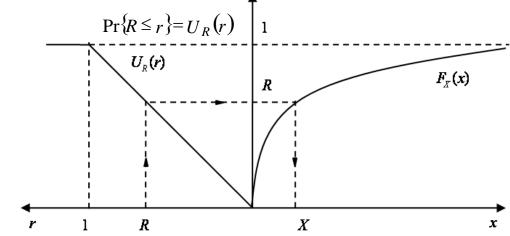
### Sampling (pseudo) random numbers from generic distribution: Inverse Transform Method





9

### Sampling (pseudo) random numbers from generic distribution: Inverse Transform Method



Sample R from  $U_R(r)$  and find X:

$$X = F_X^{-1}(R)$$

<u>Question</u>: which distribution does X obey?  $P\{X \le x\} = P\{F_x^{-1}(R) \le x\}$ 

Application of the operator  $F_x$  to the argument of P above yields  $P\{X \le x\} = P\{R \le F_X(x)\} = F_X(x)$ 

<u>Summary</u>: From an R ~  $U_R(r)$  we obtain an X ~  $F_X(x)$ 

ໄດ້ໄດ້

POLITECNICO

### Buffon's needle: MC simulation with inverse transform method

- Initialize the counter of the number of times the needle intercepts a line:  $N_s = 0$
- Simulate N > > 1 needle throws by
  - Sampling Y from the uniform distribution in the interval [0,D]:  $f_Y(y) = \frac{1}{D}$   $y \in [0,D]$

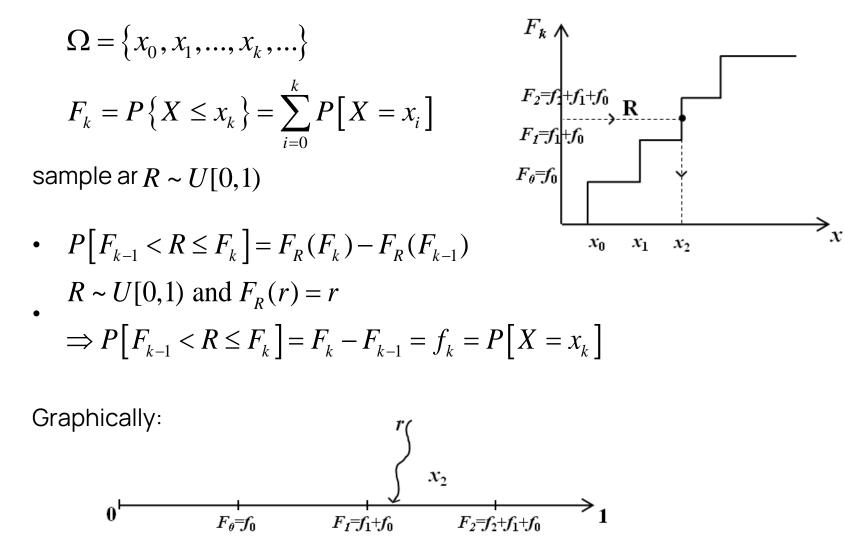
by using the inverse transform method:

- Sampling  $\Theta$  from the uniform distribution in the interval  $[0,\pi]$  by using the inverse transform method:  $\Theta = R_2\pi$
- If the needle intercepts a line, i.e.  $Y \leq Lsin\Theta$ , set  $N_s = N_s + 1$
- At the end of the procedure:  $P = \frac{N_s}{N} \cong \frac{2L}{\pi D}$

ໄດ້ໄດ້

POLITECNICO

### Sampling by the Inverse Transform Method: Discrete Distributions





12

### Sampling by the Inverse Transform Method: Exponential Distribution

- Markovian system with two states (good, failed)
- hazard rate,  $\lambda$  = constant
- Cdf  $F_T(t) = P\{T \le t\} = 1 e^{-\lambda t}$
- •pdf  $f_T(t) \cdot dt = P\{t \le T < t + dt\} = \lambda e^{-\lambda t} \cdot dt$
- Sampling a failure time T

$$R \equiv F_R(r) = F_T(t) = 1 - e^{-\lambda t}$$
$$\bigcup$$
$$T = F_T^{-1}(R) = -\frac{1}{\lambda} \ln(1 - R)$$



### Sampling by the Inverse Transform Method: Weibull Distribution

cdf: 
$$F_T(t) = P\{T \le t\} = 1 - e^{-\beta t^{\alpha}}$$
  
pdf:  $f_T(t) \cdot dt = P\{t \le T < t + dt\} = \alpha \beta t^{\alpha - 1} e^{-\beta t^{\alpha}} \cdot dt$ 

• Sampling a failure time T

$$R \equiv F_R(r) = F_T(t) = 1 - e^{-\lambda t^{\alpha}}$$

$$\int_{T} T = F_T^{-1}(R) = \left(-\frac{1}{\beta}\ln(1-R)\right)^{\frac{1}{\alpha}}$$



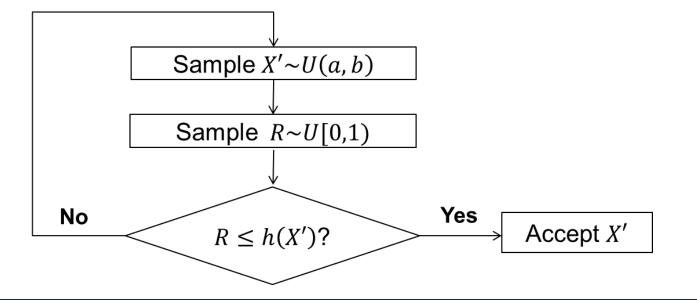
• Given a pdf  $f_X(x)$  limited in (a,b), let

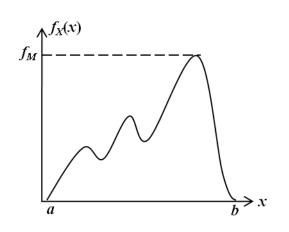
$$h(x) = \frac{f_X(x)}{f_M}$$

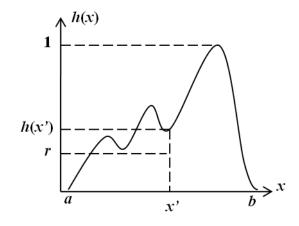
so that

 $0 \le h(x) \le 1, \forall x \in (a, b)$ 

• The operative procedure







lasar

POLITECNICO MILANO 1863

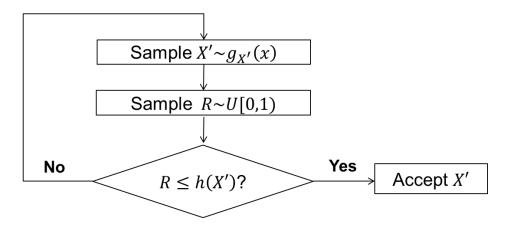
More generally:

$$X \sim f_X(x) = g_{X'}(x) \cdot H(x)$$
$$B_H : \max_x H(x)$$
$$h(x) = \frac{H(x)}{B_H}, \ 0 \le h(x) \le 1$$

The operative procedure:

- sample X'~ $g_{X'}(x)$ , and calculate h(X')
- sample R ~U[0,1). If R < =h(X') the value X' is accepted; else start again.

 $g_{X'}(x)$  is a distribution it is easy to sample from (uniform, normal, ...) H(x) is a shape correction factor f(x)/g(x)



ໄດ້ໄດ້

POLITECNICO

We show that the accepted value is actually a realization of X sampled from  $f_{\rm X}({\rm x})$ 

$$P[X' \le x | \text{ accepted}] = \frac{P[X' \le x \cap \text{ accepted}]}{P[\text{ accepted}]} = \frac{P[X' \le x \cap R \le h(X')]}{P[\text{ accepted}]}$$

$$P[z \le X' \le z + dz \cap \text{accepted}] = P[z \le X' \le z + dz]P[R \le h(z)] =$$
$$= g_{X'}(z)dz \cdot h(z)$$

3.

4.

2.

$$P[X' \le x \cap R \le h(X')] = \int_{-\infty}^{x} g_{X'}(z) dz \cdot h(z)$$
$$P[\text{accepted}] = \int_{-\infty}^{\infty} g_{X'}(z) dz \cdot h(z) =$$
$$= \frac{1}{B_{H}} \int_{-\infty}^{\infty} g_{X'}(z) dz \cdot H(z) = \frac{1}{B_{H}} \int_{-\infty}^{\infty} f_{X}(x) dx = \frac{1}{B_{H}}$$



$$P\left[X \le x | \text{accepted}\right] = \frac{P\left[X \le x \cap R \le h(x')\right]}{P[\text{accepted}]} = \frac{\int_{-\infty}^{x} g_{X'}(z)dz \cdot h(z)}{\frac{1}{B_{H}}}$$
$$= \int_{-\infty}^{x} g_{X'}(z)dz \cdot H(z) = \int_{-\infty}^{x} f_{X}(z)dz = F_{X}(x)$$

The efficiency of the method is given by the probability of accepted:

$$\varepsilon = P[\text{accepted}] = \int_{-\infty}^{\infty} g_{X'}(z)h(z)dz = \frac{1}{B_{H}}$$



Sample from the pdf:  $f_X$ 

$$f_{x}(x) = \frac{2}{\pi} \cdot \frac{1}{(1+x)\sqrt{x}} \quad 0 \le x \le 1$$



The operative procedure:

• sample 
$$R_1 \sim U[0,1) \Longrightarrow X' = R_1^2$$
 and  $h(X') = \frac{1}{1 + R_1^2}$ 

• sample  $R_2 \sim U[0,1)$ . If  $R_2 \leq h(X')$  accept X = X'; else start again

The efficiency of the method is:

$$\varepsilon = \frac{1}{B_H} = \frac{\pi}{4} = 78.5\%$$

### CONTENTS

Sampling

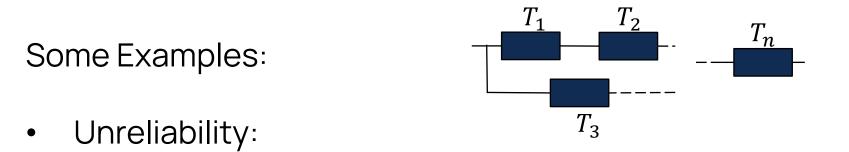
Evaluation of definite integrals

Simulation of system transport

Simulation for reliability/availability analysis



### RAM quantities of interest are definite integrals



$$F_T(t_{miss}) = P\{T \le t_{miss}\} = P\{q(T_1, \dots, T_n) \le t_{miss}\} = \int_{(t_1, \dots, t_n): q(t_1, \dots, t_n) \le t_{miss}} f_{T_1, \dots, T_n}(t_1, \dots, t_n) dt_1 \dots dt_n$$

• 
$$MTTF = \int_0^{+\infty} t f_T(t) dt$$



### MC Evaluation of Definite Integrals (1D)

•

٠

$$G = \int_{a}^{b} h(x)dx = \int_{a}^{b} g(x)f_{X}(x)dx$$

$$\downarrow$$

$$x \text{ is a random variable with pdf } f_{X}(x): \begin{cases} f_{X}(x) \ge 0\\ \int_{a}^{b} f_{X}(x)dx = \end{cases}$$

$$\downarrow$$

$$E[g(x)] = \int_{a}^{b} g(x)f_{X}(x)dx = G$$



1

### MC Evaluation of Definite Integrals (1D)

$$G = \int_{a}^{b} g(x) f(x) dx = E[g(x)]$$

**Problem**  $\rightarrow$  Estimate E[g(x)]

#### Solution → Dart Game

1) for i = 1, 2, ..., N  $\circ$  Sample  $X_i$  from  $f_X(x)$  (the probability that a shot hits  $x \in dx$  is f(x)dx)  $\circ$  Compute  $g(X_i)$  (the award is g(x)) End Consider N trials with results  $\{x_1, x_2, ..., x_N\}$ : the average award is:  $G_N = \frac{1}{N} \sum_{i=1}^N g(x_i) = \overline{g}$ Random variable!  $E[G_N] \checkmark Var[G_N]$ Is  $G_N$  a good estimator of E[g(x)]?



lasar

POLITECNICO

### MC Evaluation of Definite Integrals (1D): Why $G_N$ is a good estimator of *G*? $G_N = \frac{1}{N} \sum_{i=1}^N g(x_i)$

 $G_N$  is a random variable with:

$$E[G_N] = E\left[\frac{1}{N}\sum_{i=1}^N g(x_i)\right] = \frac{1}{N}\sum_{i=1}^N E[g(x)] = G$$

$$Var[G_N] = Var\left[\frac{1}{N}\sum_{i=1}^N g(x_i)\right] = \frac{1}{N^2}\sum_{i=1}^N Var[g(x)] = \frac{1}{N}Var[g(x)]$$

$$\bigcirc$$

$$G_N \text{ is an unbiased estimator of } G: \quad E[G_N] = G$$

$$G_N \text{ is a consistent estimator of } G: \quad \lim_{N \to \infty} Var[G_N] = 0$$

$$G = \int_0^1 \cos\left(\frac{\pi}{2}x\right) dx = \frac{2}{\pi} = 0.6366$$

# How can we write the integral for MC estimation?

$$f(x) = ?$$
  $g(x) = ?$ 



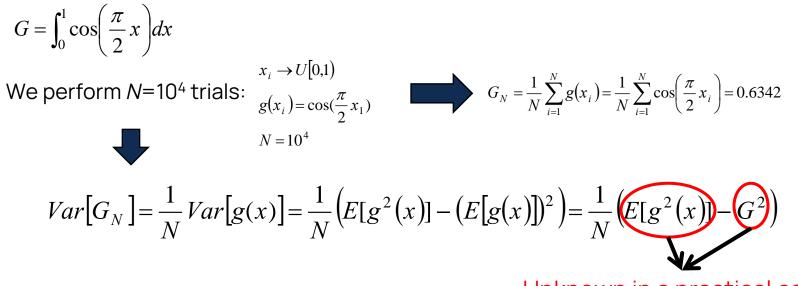
$$G = \int_0^1 \cos\left(\frac{\pi}{2}x\right) dx = \frac{2}{\pi} = 0.6366$$

By setting:

$$f(x) = 1 \quad for \quad x \in [0,1]$$
$$g(x) = \cos\left(\frac{\pi}{2}x\right)$$

We perform  $N=10^4$  trials:



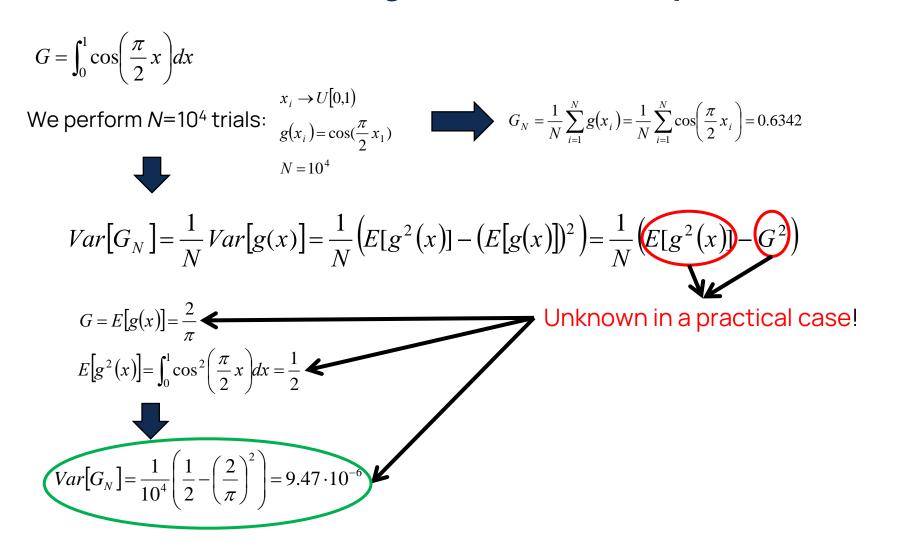


Unknown in a practical case!



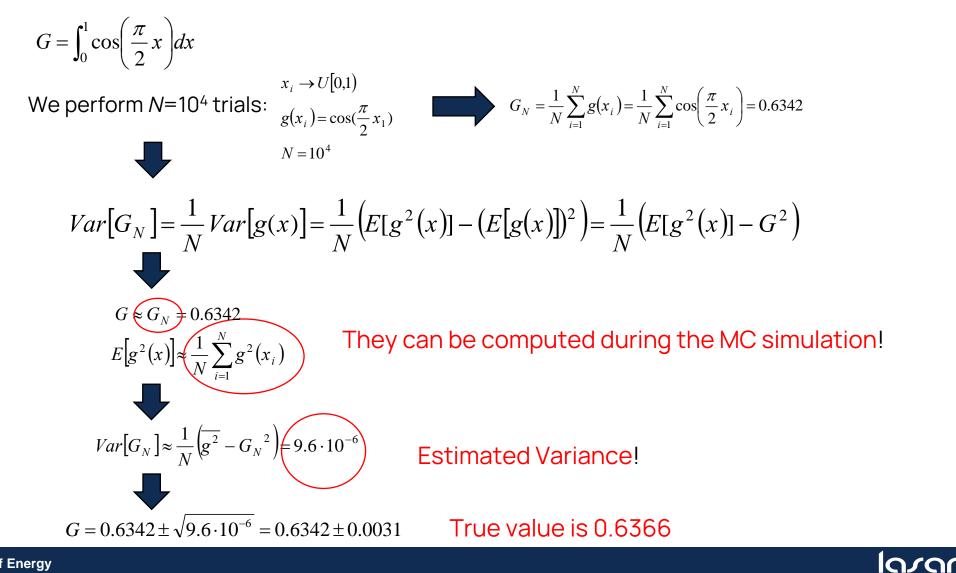
ได้วัดท

POLITECNICO



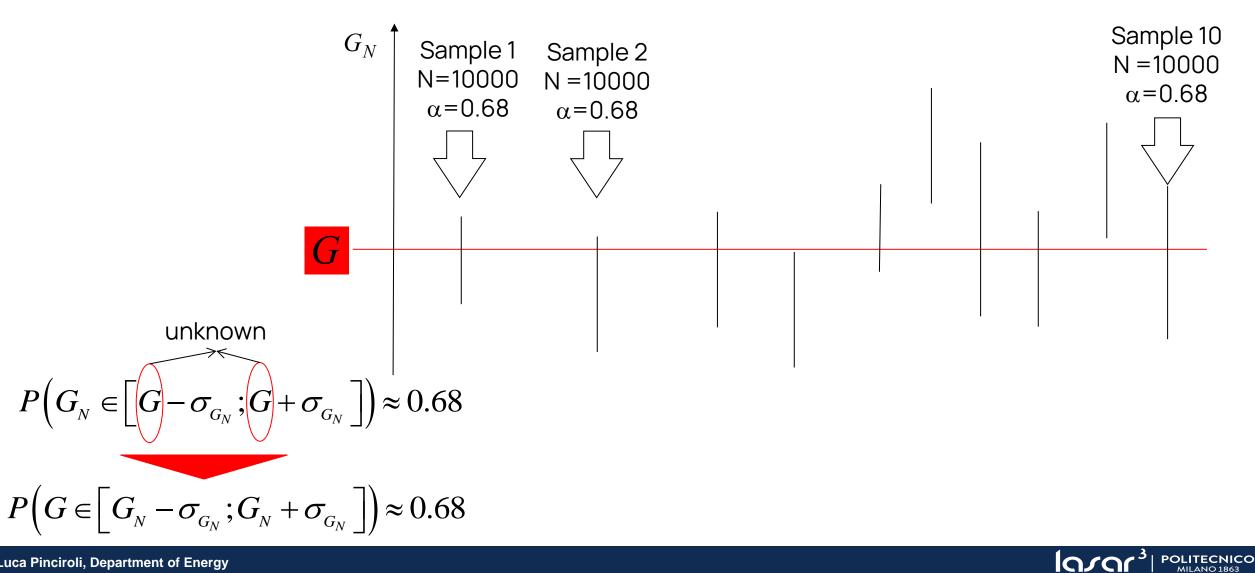


29



POLITECNICO

### MC Integral: interpretation of the variance



# Definite Integral – Monte Carlo Vs Deterministic Numerical Integration

Why Monte Carlo instead of deterministic numerical integration?

Because the latter suffers from two major issues when dealing with highly multidimensional problems:

- 1. The number of function evaluations (grid) increases combinatorially with the number of dimensions
- 2. The boundaries of the multidimensional integration domain *D* become intractable



#### **Estimation error – variance reduction**

- The estimate  $G_N$  becomes more precise (less uncertain) as the estimator variance  $Var[G_N]$  decreases!
- How can we achieve lower  $Var[G_N] = \frac{1}{N} Var[g(x)]$ ?
  - 1. Increasing the number N of MC trials  $\Rightarrow$  "brute force"
  - 2. Decreasing  $Var[g(x)] \Rightarrow$  variance reduction techniques

$$G = \int_{D} \left[ \frac{f(x)}{f_1(x)} g(x) \right] f_1(x) dx \equiv \int_{D} g_1(x) f_1(x) dx$$

Forced (biased) MC simulation



# MC estimation of RAM quantities of interest: Unreliability estimation example

T = System failure time

 $T_i \approx f_{T_i}(t_i) = Component failure time$ 

$$F_{T}(t)??? = \begin{bmatrix} T_{1} & T_{2} & T_{1} \approx f_{T_{1}}(t_{1}) \\ T_{2} \approx f_{T_{2}}(t_{2}) \end{bmatrix}$$

$$F_T(t_{miss}) = P\{T \le t_{miss}\} =$$
$$= \int_0^{t_{miss}} f_T(t) dt = \int_0^{+\infty} I_g(t) f_T(t) dt$$

with

$$I_g(t) = \begin{cases} 1 & if \ t \le t_{miss} \\ 0 & otherwise \end{cases}$$

$$G = \int_{a}^{b} g(x)f(x)dx = E[g(x)]$$
  

$$G = F_{T}(t_{miss}) \quad g(x) = I_{g}(t) \quad f(x) = f_{T}(t)$$

T is evaluated by means of MC simulation

$$F_T(t_{miss}) = P\{T \le t_{miss}\} =$$

$$= \int_0^{t_{miss}} f_T(t) dt = \int_0^{+\infty} I_g(t) f_T(t) dt$$

$$I_g(t) = 1 \qquad I_g(t) = 0$$

$$t_{miss} \qquad t$$

ได้วัดเ

POLITECNICO

# MC estimation of RAM quantities of interest: Unreliability estimation example

$$\begin{array}{cccc} T_1 & T_2 & f_{T_1}(t) = \lambda_1 e^{-\lambda_1 t} & t_{miss} = 8760 \ h \\ f_{T_2}(t) = \lambda_2 e^{-\lambda_2 t} & \lambda_1 = 210^{-4} \ h^{-1} \\ \lambda_2 = 510^{-3} \ h^{-1} \end{array} \begin{array}{c} \text{OBJECTIVE:} \\ \text{MC Estimate System Unreliability} \\ \text{at the Mission Time} \end{array}$$

# MC estimation of RAM quantities of interest: Unreliability estimation example

$$\begin{array}{cccc} T_1 & T_2 & f_{T_1}(t) = \lambda_1 e^{-\lambda_1 t} & t_{miss} = 8760 \ h \\ f_{T_2}(t) = \lambda_2 e^{-\lambda_2 t} & \lambda_1 = 210^{-4} \ h^{-1} \\ \lambda_2 = 510^{-3} \ h^{-1} \end{array} \begin{array}{c} \text{OBJECTIVE:} \\ \text{MC Estimate System Unreliability} \\ \text{at the Mission Time} \end{array}$$

$$N = 10000 \Rightarrow \lambda_{sys} = \lambda_1 + \lambda_2 \Rightarrow for \ i = 1, ..., N \Rightarrow t_i = -\frac{1}{\lambda_{sys}} \ln(1 - r_i), r_i \Rightarrow U[0, 1)$$

$$F_N(t_{miss}) = \frac{1}{N} \sum_{i=1}^N I_g(t_i) = 0,9891 \quad where \quad I_g(t_i) = \begin{cases} 1 & if \ t_i < t_{miss} \\ 0 & otherwise \end{cases}$$

$$Var[F_N(t_{miss})] \approx \frac{1}{N} \left( \left( \frac{1}{N} \sum_{i=1}^N \left( I_g(t_i) \right)^2 \right) - F_N^2(t_{miss}) \right) \approx \frac{1}{N} \left( F_N(t_{miss}) - F_N^2(t_{miss}) \right) = 1,08 \ 10^{-6}$$

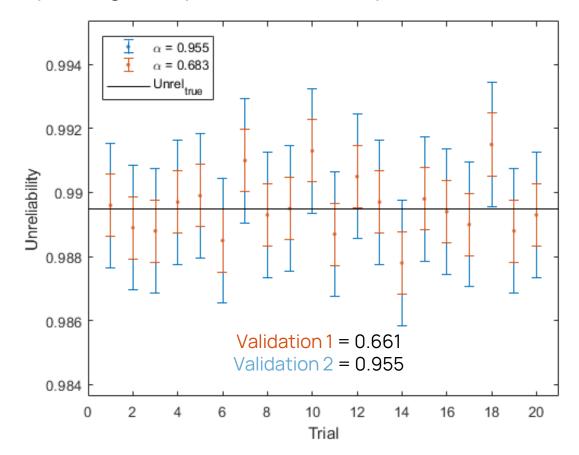
MC ESTIMATION OF SYSTEM UNRELIABILITY =  $F_N(t_{miss}) \pm \sqrt{Var[F_N(t_{miss})]} = 0,9891 \pm 1,0 \ 10^{-3}$ 

TRUE VALUE OF SYSTEM UNRELIABILITY =  $1 - e^{-(\lambda_1 + \lambda_2)t_{miss}} = 0,9895$ 



# MC estimation of RAM quantities of interest: Unreliability estimation example

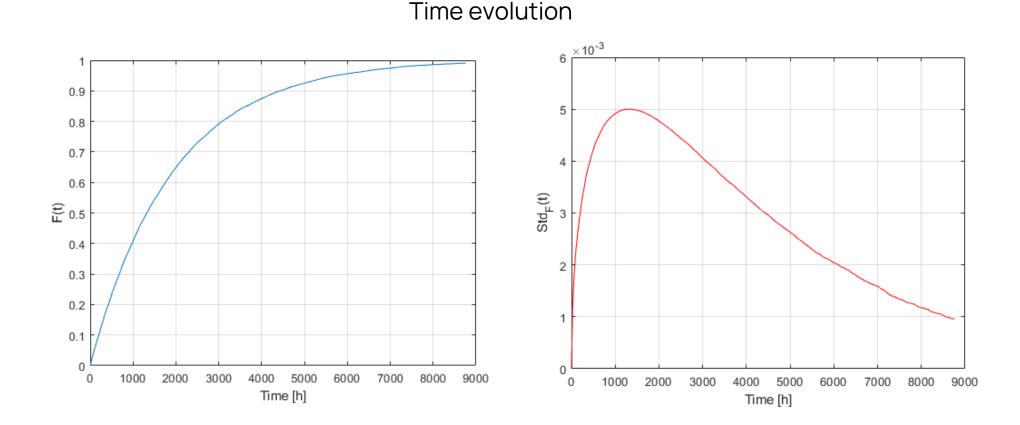
Repeating the system unreliability estimation 1000 times ...



larar

POLITECNICO MILANO 1863

# MC estimation of RAM quantities of interest: Unreliability estimation example



larar

POLITECNICO

#### MTTF estimation example

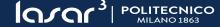
$$MTTF = \int_{0}^{+\infty} t f_{T}(t) dt$$
$$G = \int_{a}^{b} g(x)f(x)dx = E[g(x)] \qquad G = MTTF \qquad g(x) = t \qquad f(x) = f_{T}(t)$$

Exponential failure time T

$$-f_T(t) = \lambda e^{-\lambda t} \qquad \lambda = 0,2 \,\mathrm{h}^{-1}$$

OBJECTIVE: MC Estimate System MTTF





#### MTTF estimation example

G =

$$MTTF = \int_{0}^{+\infty} t f_{T}(t) dt$$
$$\int_{a}^{b} g(x)f(x)dx = E[g(x)] \qquad G = MTTF \qquad g(x) = t \qquad f(x) = f_{T}(t)$$

Exponential failure time T

$$-f_T(t) = \lambda e^{-\lambda t} \qquad \lambda = 0,2 \,\mathrm{h}^{-1}$$

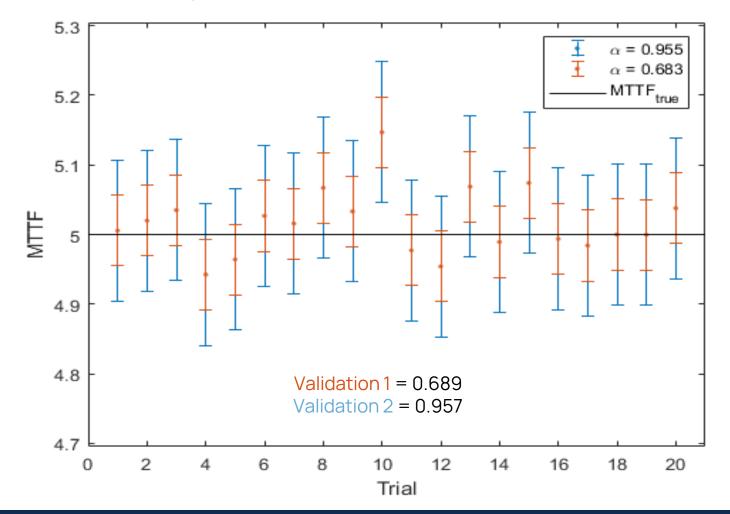
larar

POLITECNICO MILANO 1863

Considering 
$$N = 10000$$
  
trials:  
 $MTTF_N = \frac{1}{N} \sum_{i=1}^N T_i = 4,98 h$   
 $Var[MTTF_N] \approx \frac{1}{N} \left( \left( \frac{1}{N} \sum_{i=1}^N T_i^2 \right) - MTTF_N^2 \right) = 0,0024 h$   
MC ESTIMATION OF SYSTEM  $MTTF = MTTF_N \pm \sqrt{Var[MTTF_N]} = 4,98 \pm 0,049$   
TRUE VALUE OF SYSTEM  $MTTF = \frac{1}{\lambda} = 5 h$ 

#### MTTF estimation example

Repeating the system MTTF estimation 1000 times ...



larar

POLITECNICO MILANO 1863

# CONTENTS

Sampling

Evaluation of definite integrals

Simulation of system transport

Simulation for reliability/availability analysis

#### Monte Carlo simulation for system reliability

**SYSTEM** = system of Nc suitably connected components.

**COMPONENT** = a subsystem of the system (pump, valve,...) which may stay in different exclusive (multi)states (nominal, failed, stand-by,...). Stochastic transitions from state-to-state occur at stochastic times.

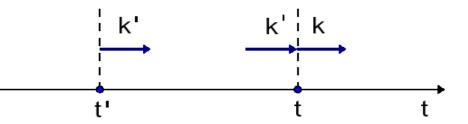
**STATE of the SYSTEM** at t = the set of the states in which the Nc components stay at t. The states of the system are labeled by a scalar which enumerates all the possible combinations of all the component states.

**SYSTEM TRANSITION** = when any one of the plant components performs a state transition we say that the system has performed a transition. The time at which the system performs the n-th transition is called  $t_n$  and the system state thereby entered is called  $k_n$ .

**SYSTEM LIFE** = stochastic process.



# **Stochastic Transitions: Governing Probabilities**



T(t t'; k')dt = conditional probability of a transition at  $t \in dt$ , given that the preceding transition occurred at t' and that the state thereby entered was k'.

 $C(k \mid k'; t)$  = conditional probability that the system enters state k, given that a transition occurred at time t when the system was in state k'.

```
Both these probabilities form the "trasport kernel" :

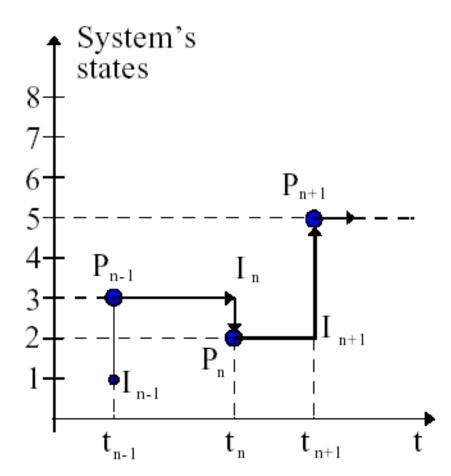
K(t; k \mid t'; k')dt = T(t \mid t'; k')dt C(k \mid k'; t)
```

 $\psi$ (t; k) = ingoing transition density or probability density function (pdf) of a system transition at t, resulting in the entrance in state k



#### System life: random walk

Random walk = realization of the system life generated by the underlying state-transition stochastic process.





#### The von Neumann's Approach and the Transport Equation

The transition density  $\psi(t; k)$  is expanded in series of the partial transition densities:

 $\psi^{n}(t; k) = pdf$  that the system performs the n-th transition at t, entering the state k.

Then,

$$\psi(t,k) = \sum_{n=0}^{\infty} \psi^{n}(t,k) =$$
  
=  $\psi^{0}(t,k) + \sum_{k'} \int_{t_{0}}^{t} dt' \psi(t',k') K(t,k \mid t',k')$ 

Transport equation for the plant states



54

## Monte Carlo Solution to the Transport Equation (1)

Von Neumann approach:

- Initial Conditions:  $t_0 = t^*$ ,  $k_0 = k^*$ ,  $P_0 \equiv P^*$
- The subsequent transition densities in the random walk:

$$\psi^{1}(t_{1},k_{1}) = K(t_{1},k_{1}|t_{0},k_{0})$$

$$\psi^{2}(t_{2},k_{2}) = \sum_{k_{1}} \int_{t^{*}}^{t_{2}} \psi^{1}(t_{1},k_{1}) dt_{1} K(t_{2},k_{2} | t_{1},k_{1})$$

• In general:

$$\psi^{n}(t_{n},k_{n}) = \sum_{k_{n-1}} \int_{t^{*}}^{t_{n}} \psi^{n-1}(t_{n-1},k_{n-1}) dt_{n-1} K(t_{n},k_{n} | t_{n-1},k_{n-1})$$

$$t_{n} \to t \qquad k_{n-1} \to k'$$

$$t_{n-1} \to t' \qquad k_{n} \to k$$

55

#### Monte Carlo Solution to the Transport Equation (2)

$$\begin{split} \psi^{n}(t,k) &= \sum_{k'} \int_{t^{*}}^{t} \psi^{n-1}(t',k') dt' K(t,k | t',k') \\ \Rightarrow \psi(t,k) &= \sum_{n=0}^{\infty} \psi^{n}(t,k) = \psi^{0}(t,k) + \\ &+ \sum_{k'} \int_{t^{*}}^{t} \sum_{\substack{n-1=0 \\ \psi(t',k')}}^{\infty} \psi^{n-1}(t',k') dt' K(t,k | t',k') \\ \left( \sum_{n-1=0}^{\infty} \psi^{n-1}(t',k') = \psi(t',k') \right) \end{split}$$



#### Monte Carlo Solution to the Transport Equation (3)

Initial Conditions: (*t\*, k\**) Formally rewrite the partial transition densities:

$$\psi^{1}(t_{1},k_{1}) = \sum_{k_{0}} \int_{t^{*}}^{t_{1}} dt_{0} \psi^{0}(t_{0},k_{0}) K(t_{1},k_{1}|t_{0},k_{0}) = K(t_{1},k_{1}|t^{*},k^{*})$$
  
$$\psi^{2}(t_{2},k_{2}) = \sum_{k_{1}} \int_{t^{*}}^{t_{2}} dt_{1} \psi^{1}(t_{1},k_{1}) K(t_{2},k_{2}|t_{1},k_{1}) =$$
  
$$= \sum_{k_{1}} \int_{t^{*}}^{t_{2}} dt_{1} K(t_{1},k_{1}|t^{*},k^{*}) K(t_{2},k_{2}|t_{1},k_{1})$$
  
.....

$$\psi^{n}(t,k) = \sum_{k_{1},k_{2},\dots,k_{n-1}} \int_{t^{*}}^{t_{n}} dt_{n-1} \int_{t^{*}}^{t_{n-1}} dt_{n-2} \dots$$
$$\dots \int_{t^{*}}^{t_{2}} dt_{1} K(t_{1},k_{1}|t^{*},k^{*}) K(t_{2},k_{2}|t_{1},k_{1}) \cdots K(t,k|t_{n-1},k_{n-1})$$

lasar

POLITECNICO

# CONTENTS

Sampling

Evaluation of definite integrals

Simulation of system transport

Simulation for reliability/availability analysis



#### **Monte Carlo Simulation in RAMS**

$$G(t) = \sum_{k \in \Gamma} \int_0^t \psi(\tau, k) R_k(\tau, t) d\tau \quad \text{Expected value}$$

- G(t): expected value representing unavailability or unreliability.
- Γ: Subset of system failure states.
- $\psi(\tau, k)$ : Probability density of entering state k at time  $\tau$ .
- $R_k(\tau, t)$ : **Residual probability** probability the system stays in failure state k until time t, after entering at  $\tau$
- $R_k(\tau, t) = 1 \Rightarrow G(t) =$ unreliability
- $R_k(\tau, t) = \text{prob. system not exiting before t from the state k entered at <math>\tau < t$  $\Rightarrow G(t) = \text{unavailability}$

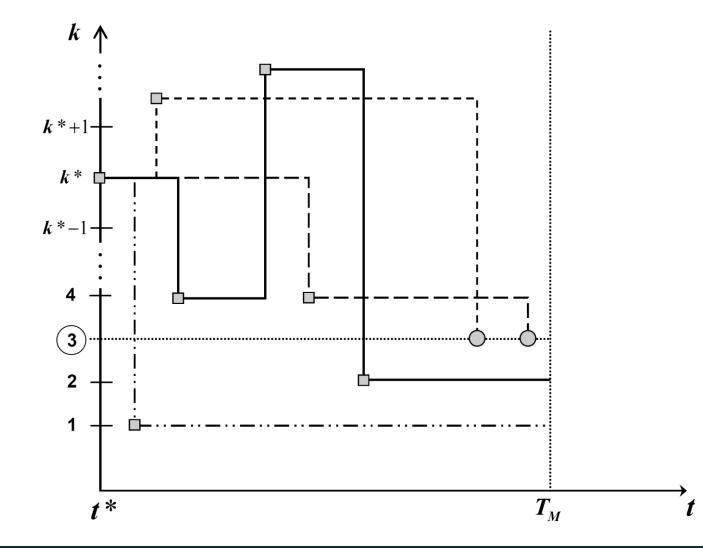
#### Monte Carlo solution of a definite integral: expected value $\cong$ sample mean

- 1. Randomly sampling system lives (random walks)
- 2. Estimating G(t) as the mean over those samples

ໄດ້ກັດເ

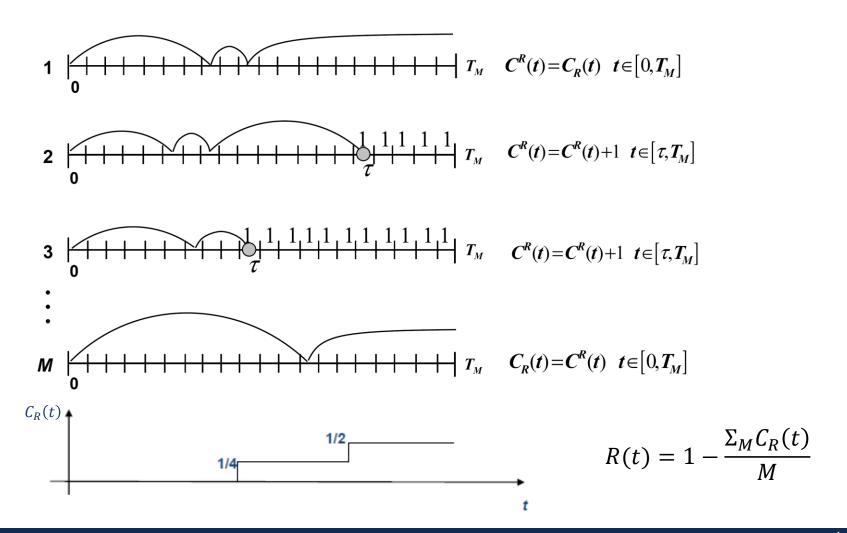
POLITECNICO

#### Phase space





#### System reliability estimation



lasar

POLITECNICO MILANO 1863

#### System availability estimation

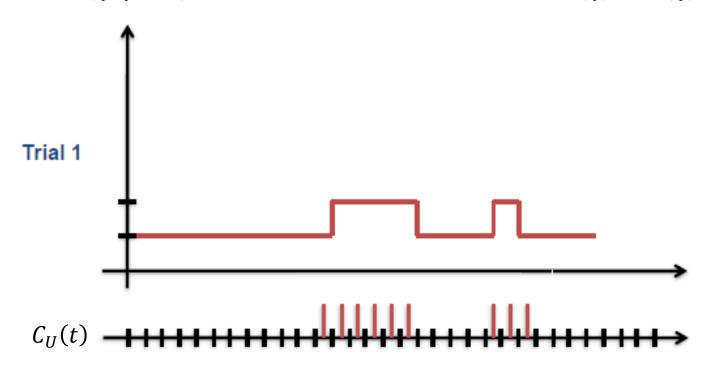
• Divide the mission time, *TM*, in bins and associate a counter (of the system failure) to each bin:

$$C_U(1), C_U(2), \dots, C_U(\tau)$$

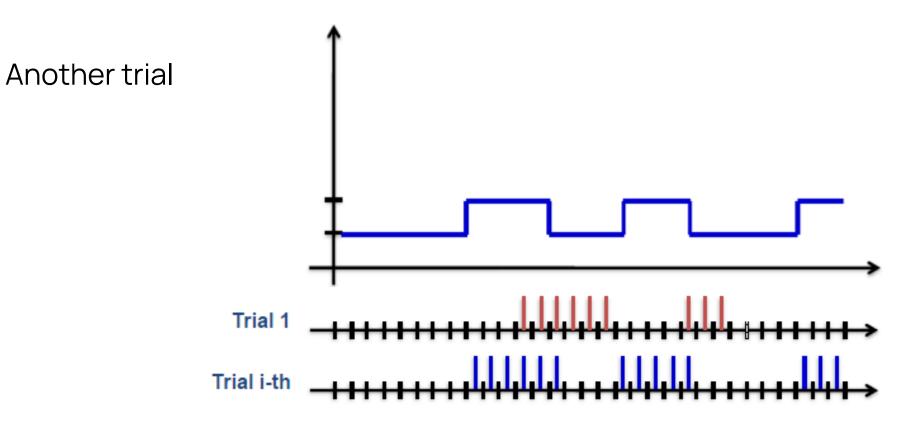
• Initialize each counter to 0:

$$C_U(1), C_U(2), \dots, C_U(\tau) = 0$$

• If the component is failed in  $(t_i, t_j + \Delta t)$ , the corresponding counter increases  $C_U(t_j) = C_U(t_j) + 1$ , otherwise  $C_U(t_j) = C_U(t_j)$ 

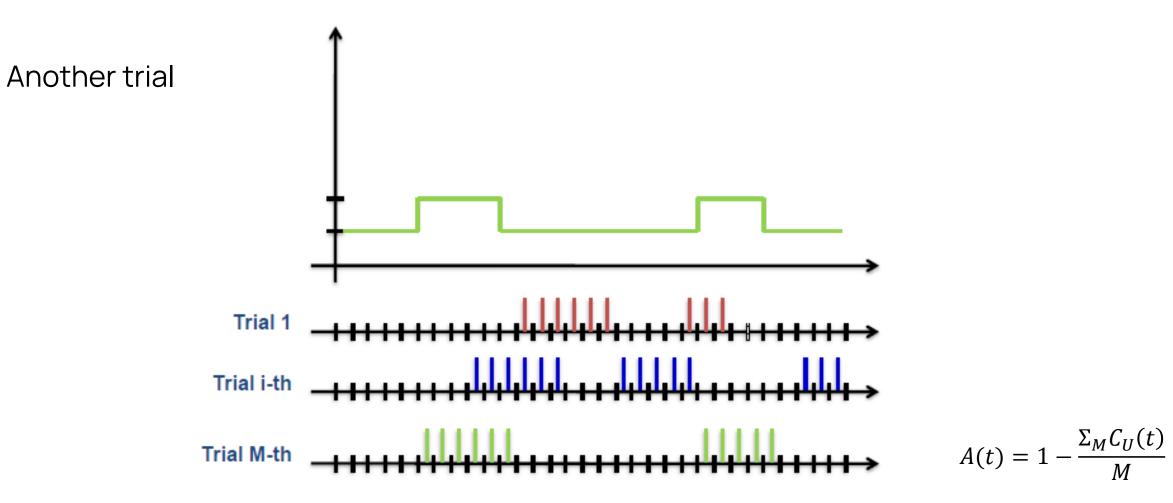


#### System availability estimation





#### System availability estimation





64



#### Monte Carlo Simulation Approaches

• Each trial of a Monte Carlo simulation consists in generating a random walk which guides the system from one configuration to another, at different times.

• During a trial, starting from a given system configuration k' at t', we need to determine when the next transition occurs and which is the new configuration reached by the system as a consequence of the transition.

• This can be done in two ways which give rise to the so called "<u>indirect</u>" and "<u>direct</u>" Monte Carlo approach.



#### **Indirect Monte Carlo**

The indirect approach consists in:

- 1. Sampling first the time t of a system transition from the corresponding conditional probability density T(t|t',k') of the system performing one of its possible transitions out of k' entered at time t'.
- 2. Sampling the transition to the new configuration k from the conditional probability C(k|t,k') that the system enters the new state k given that a transition has occurred at t starting from the system in state k'.
- 3. Repeating the procedure from k' at time t to the next transition.

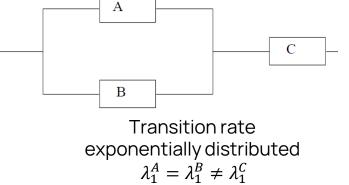


#### Indirect Monte Carlo: Example

#### SAMPLING THE TIME OF TRANSITION

The rate of transition of component A(B) out of its nominal state 1 is:

$$\lambda_1^A = \lambda_1^B$$



lasar

POLITECNICO

• The rate of transition of component C out of its nominal state 1 is:

 $\lambda_1^C$ 

•The rate of transition of the system out of its current configuration (1 1, 1) is:  

$$\lambda^{(1,1,1)} = \lambda_1^A + \lambda_1^B + \lambda_1^C$$

•We are now in the position of sampling the first system transition time  $t_1$ , by applying the inverse transform method:

$$t_1 = t_0 - \frac{1}{\lambda^{(1,1,1)}} \ln(1 - R_t)$$

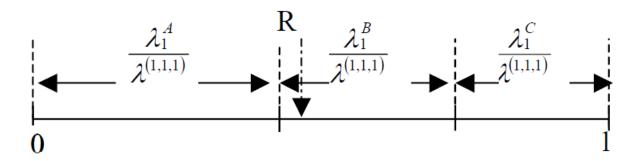
where  $R_t \sim U[0,1)$ 

#### Indirect Monte Carlo: Example

- Assuming that t<sub>1</sub> < T<sub>M</sub> (otherwise we would proceed to the successive trial), we now need to determine which transition has occurred, i.e. which component has undergone the transition and to which arrival state.
- The probabilities of components A, B, C undergoing a transition out of their initial nominal states 1, given that a transition occurs at time t<sub>1</sub>, are:

$$rac{\lambda_1^A}{\lambda^{(1,1,1)}}, \quad rac{\lambda_1^B}{\lambda^{(1,1,1)}}, \quad rac{\lambda_1^C}{\lambda^{(1,1,1)}}$$

 Thus, we can apply the inverse transform method to the discrete distribution





## Direct Monte Carlo (1)

The <u>direct approach</u> differs from the previous one in that the system transitions are not sampled by considering the distributions for the whole system but rather by sampling directly the times of all possible transitions of all individual components of the system and then arranging the transitions along a timeline, in accordance to their times of occurrence. Obviously, this timeline is updated after each transition occurs, to include the new possible transitions that the transient component can perform from its new state. In other words, during a trial starting from a given system configuration k' at t':

- 1. We sample the times of transition  $t_{j' \to m_i}^i$ ,  $m_i = 1, 2, ..., N_{S_i}$ , of each component *i*,  $i = 1, 2, ..., N_c$ leaving its current state  $j'_i$  and arriving to the state  $m_i$  from the corresponding transition time probability distributions  $f_T^{i,j_i \to m_i}(t|t')$ .
- 2. The time instants  $t_{j_i \to m_i}^i$  thereby obtained are arranged in ascending order along a timeline from  $t_{min}$  to  $t_{max} \le T_{M}$ .

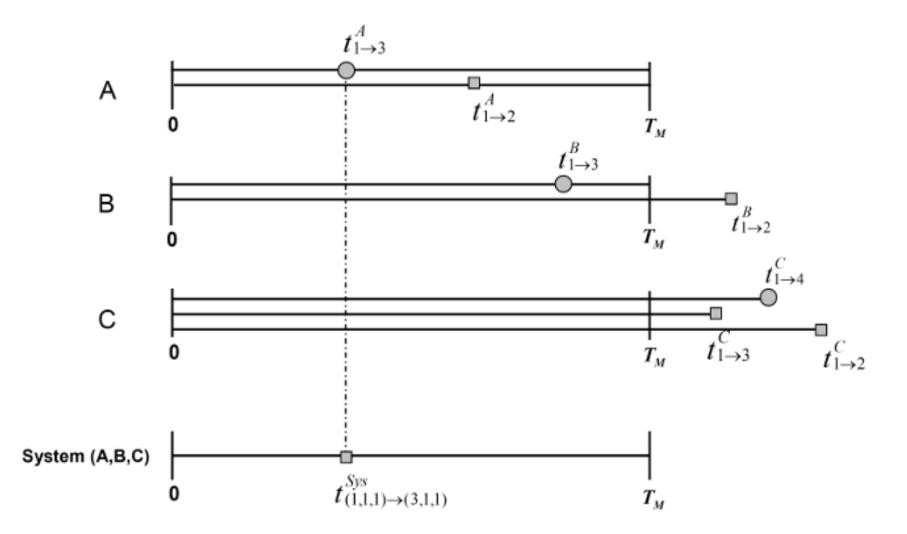
## Direct Monte Carlo (2)

- 3. The clock time of the trial is moved to the first occurring transition time  $t_{min} = t^*$  in correspondence of which the system configuration is changed, i.e. the component *i*\* undergoing the transition is moved to its new state  $m_i^*$ .
- 4. At this point, the new times of transition  $t_{m_i^* \to l_i^*}^{i^*}$ ,  $l_i^* = 1, 2, ..., N_S^{i^*}$ , of component *i*\* out of its current state  $m_i^*$  are sampled from the corresponding transition time probability distributions,  $f_T^{i^*,m_i^* \to l_i^*}(t|t^*)$ , and placed in the proper position of the timeline.
- 5. The clock time and the system are then moved to the next first occurring transition time and corresponding new configuration, respectively.
- 6. The procedure repeats until the next first occurring transition time falls beyond the mission time, i.e.  $t_{min} > T_M$ .

Compared to the previous indirect method, the direct approach is more suitable for systems whose components' failure and repair behaviours are represented by different stochastic distribution laws.



#### **Direct Monte Carlo: Example**



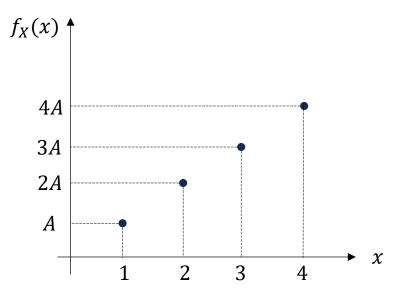


71

#### Exercise

Consider the discrete probability distribution  $f_X(x)$  in the graph:

- 1) Identify the value of the parameter A;
- 2) Compute the corresponding cumulative distribution;
- 3) Write an algorithm to sample N=1000 values from  $f_X(x)$  and evaluate the distribution of the obtained samples;



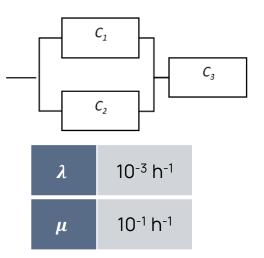


#### **Exercise: Indirect Monte Carlo**

Consider the system in the Figure, which is made up of the three binary components.

The (failure) transition from the state 'WORKING' to the state 'FAILED' is described by the constant failure rate  $\lambda$ , whereas the (repair) transition from the state 'FAILED' to the state 'WORKING' by the constant repair rate  $\mu$ , whose numerical values are reported in the Table below. The system mission time is Tm=1000 h and the components initial state at time t = 0 h are C1='WORKING', C2=' FAILED', C3='WORKING'.

- 1) Draw a possible life of the system in the phase space and indicate the states of the system which correspond to a system failure.
- 2)Compute the first transition time using the inverse transform method. Use  $R_1$ =0.232 as random number sampled from an uniform distribution in the range [0,1).
- 3) Find the state entered by the system as a result of the first transition. Use  $R_2=0.787$  as random number sampled from an uniform distribution in the range [0,1).
- 4)Simulate one entire plant life using the random numbers attached, sampled from an uniform distribution in the range [0,1). Start the simulation from the time and the state found in point Q1.3) and Q1.4), respectively.



1) 0.8929	15)0.6454	29)0.4033
2) 0.3320	16)0.9902	30)0.2170
3) 0.8212	17)0.8199	31)0.7173
4) 0.0417	18)0.4132	
5) 0.1077	19)0.8763	
6) 0.5951	20)0.8238	
7) 0.5298	21)0.0545	
8) 0.4188	22)0.7186	
9) 0.3354	23)0.8022	
10)0.6225	24)0.7364	
11) 0.4381	25)0.7091	
12)0.7359	26)0.5409	
13)0.5180	27)0.1248	
14)0.5789	28)0.9576	
	2) 0.3320 3) 0.8212 4) 0.0417 5) 0.1077 6) 0.5951 7) 0.5298 8) 0.4188 9) 0.3354 10)0.6225 11) 0.4381 12)0.7359 13)0.5180	2) 0.332016)0.99023) 0.821217)0.81994) 0.041718)0.41325) 0.107719)0.87636) 0.595120)0.82387) 0.529821)0.05458) 0.418822)0.71869) 0.335423)0.802210)0.622524)0.736411) 0.438125)0.709112)0.735926)0.540913)0.518027)0.1248

ໄດ້ໄດ້

POLITECNICO



#### References



2 Springer

2013, 2013, XIV, 198 p. 69 illus., 24 in color.

#### Printed book

- Hardcover
- ► 129,95 € | £117.00 | \$179.00
- ► \*139,05 € (D) | 142,94 € (A) | CHF 173.00

#### eBook

- For individual purchases buy at a lower price on <u>springer.com</u>. <u>A free preview is available</u>. Also available from libraries offering Springer's eBook Collection.
- springer.com/ebooks

#### 🦉 МуСору

Printed eBook exclusively available to patrons whose library offers Springer's eBook Collection.\*\*\* ► € | \$ 24.95

- P C 3 24.3
- springer.com/mycopy

#### E. Zio, Ecole Centrale Paris, Chatenay-Malabry, France <u>The Monte Carlo Simulation Method for System Reliability and</u> Risk Analysis

Series: Springer Series in Reliability Engineering

springer.com

- Illustrates the Monte Carlo simulation method and its application to reliability and system engineering to give the readers the sound fundamentals of Monte Carlo sampling and simulation
- Explains the merits of pursuing the application of Monte Carlo sampling and simulation methods when realistic modeling is required so that readers may exploit these in their own applications
- Includes a range of simple academic examples in support to the explanation of the theoretical foundations as well as case studies provide the practical value of the most advanced techniques so that the techniques are accessible

Monte Carlo simulation is one of the best tools for performing realistic analysis of complex systems as it allows most of the limiting assumptions on system behavior to be relaxed. The Monte Carlo Simulation Method for System Reliability and Risk Analysis comprehensively illustrates the Monte Carlo simulation method and its application to reliability and system engineering. Readers are given a sound understanding of the fundamentals of Monte Carlo sampling and simulation and its application for realistic system modeling.

Whilst many of the topics rely on a high-level understanding of calculus, probability and statistics, simple academic examples will be provided in support to the explanation of the theoretical foundations to facilitate comprehension of the subject matter. Case studies will be introduced to provide the practical value of the most advanced techniques.

This detailed approach makes The Monte Carlo Simulation Method for System Reliability and Risk Analysis a key reference for senior undergraduate and graduate students as well as researchers and practitioners. It provides a powerful tool for all those involved in system analysis for reliability, maintenance and risk evaluations.



Order online at springer.com > or for the Americas call (toll free) 1-800-SPRINGER > or email us at: ordersny@springer.com. > For outside the Americas call +49 (0) 6221-345-4301 > or email us at: orders-hd-individuals@springer.com.

The find grace and the E and S price are ent prices, subject to local VRL. Prices indicated with " include WRT for books, the 4(b) include 78 for Gennary, the 4(b) includes 10% for Austria. Prices includes indicated with " include VRT for electronic products; 10% for Gennary, 20% for Austra. All prices exalates of catalyce changes. Ricces and other details are subject to change without notics. All errors and catalyces excepted.

\*\*\* Regional restrictions apply



74

# Thank you for your kind attention



#### Contacts

Building B12 Campus Bovisa, Via La Masa 34, 20156, Milan, Italy. 02 2399 6349 Iuca.pinciroli@polimi.it www.lasar.polimi.it

